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**Geometrical Product Specifications
(GPS) — Filtration
Part 32 Robust Profile Filters Spline
Filters**

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NATIONAL FOREWORD

This Indian Standard (Part 32) which is identical to ISO/TR 16610-32 : 2023 'Geometrical product specifications (GPS) — Filtration — Part 32: Robust profile filters: Spline filters' issued by the International Organization for Standardization (ISO) was adopted by the Bureau of Indian Standards on recommendation of the Engineering Metrology Sectional Committee and approval of the Production and General Engineering Division Council.

This part specifies the terminology and concepts for spline filters. Spline filters have the advantage of being implementable for non-uniform sampling positions and for closed profiles.

This standard has been published in several parts, other parts in this series are:

- Part 1 Overview and basic concepts
- Part 20 Linear profile filters: Basic concepts
- Part 21 Linear profile filters: Gaussian filters
- Part 22 Linear profile filters: Spline filters
- Part 28 Profile filters: End effects
- Part 29 Linear profile filters: Wavelets
- Part 30 Robust profile filters: Basic concepts
- Part 31 Robust profile filters: Gaussian regression filters
- Part 40 Morphological profile filters: Basic concepts
- Part 41 Morphological profile filters: Disk and horizontal line-segment filters
- Part 49 Morphological profile filters: Scale space techniques
- Part 60 Linear areal filters: Basic concepts
- Part 61 Linear areal filters: Gaussian filters
- Part 62 Linear areal filters: Spline filters
- Part 71 Robust areal filters: Gaussian regression filters
- Part 85 Morphological areal filters: Segmentation

The text of ISO Standard has been approved as suitable for publication as an Indian Standard without deviations. Certain conventions are, however, not identical to those used in Indian Standards. Attention is particularly drawn to the following:

- a) Wherever the words 'International Standard' appear referring to this standard, they should be read as 'Indian Standard'; and
- b) Comma (,) has been used as a decimal marker while in Indian Standards, the current practice is to use a point (.) as the decimal marker.

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Introduction

This document develops the terminology and concepts for spline filters. Spline filters have the advantage of being implementable for non-uniform sampling positions and for closed profiles. An example of application of spline filters is given in [Annex A](#).

Robust filters are tolerant against outliers. Spline filters offer one method for form removal.

For more detailed information of the relation of this document to the filtration matrix and the ISO GPS standards, see [Annex B](#) and [Annex C](#).

Indian Standard

GEOMETRICAL PRODUCT SPECIFICATIONS (GPS) — FILTRATION

PART 32 ROBUST PROFILE FILTERS SPLINE FILTERS

1 Scope

This document provides information on a generalized version of the linear spline filter for uniform and non-uniform sampling and the robust spline filters for surface profiles. It supplements ISO 16610-22, ISO 16610-30 and ISO 16610-31.

This document provides information on how to apply the robust estimation to the spline filter as specified in ISO 16610-22, as well as its generalized form for non-uniform sampling. The weight function chosen for the M-estimator is the Tukey biweight influence function as specified in ISO 16610-31.

2 Normative references

There are no normative references in this document.

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <https://www.electropedia.org/>

3.1

robust filter

filter that is insensitive against specific phenomena in the input data

Note 1 to entry: A robust filter is a filter that delivers output data with robustness.

Note 2 to entry: Robust filters are nonlinear filters.

[SOURCE: ISO 16610-31:2016, 3.1, modified — Definition revised and notes to entry added.]

3.2

spline

linear combination of piecewise polynomials, with a smooth fit between the pieces

[SOURCE: ISO 16610-22:2015, 3.1, modified — Note 1 to entry removed.]

3.3

spline filter

linear filter based on *splines* (3.2)

Note 1 to entry: An example of spline filter application is given in [Annex A](#).

3.4

robust spline filter

robust filter (3.1) based on *splines* (3.2)

**3.5
uniform sampling**

sampling of data points at equidistant positions, i.e. with the width of spacing intervals between neighbouring probing points being constant

**3.6
non-uniform sampling**

sampling of data points with non-equidistant spacing points

**3.7
robust statistical estimator**

rule that indicates how to calculate an estimate based on sample data from a population that is insensitive against specific phenomena in the input data

Note 1 to entry: An example of specific phenomena is significant deviation of the distribution of the input data (amplitude distribution in the case of surface profiles) from a Gaussian distribution mostly in the form of long tails.

**3.8
M-estimator**

robust statistical estimator (3.7) which uses an influence function, i.e. a function which is asymmetric and scale invariant, to weight points according to their signed distance from the reference line

[SOURCE: ISO 16610-30:2015, 3.5, modified — Definition revised.]

**3.9
Tukey's biweight influence function**

influence function which suppresses specific phenomena in the input data x and is defined by:

$$\psi(x) = \begin{cases} x \left(1 - \left(\frac{x}{c} \right)^2 \right)^2 & \text{for } |x| \leq c \\ 0 & \text{for } |x| > c \end{cases}$$

where c is a scale parameter

4 Spline filter for uniform and non-uniform sampling

4.1 General

The following low-pass filter equation for spline profile filters is based on cubic splines with a regularization parameter depending on the nesting index, which complies with the cut-off wavelength in the case of linear filters, for the smoothness of the resultant waviness profile (low-passed signal) and a tension parameter influencing the slope of the transfer function.

4.2 Filter equation for cubic spline filter

4.2.1 General

The filter equation is given in [Formula \(1\)](#):

$$\mathbf{w} = \left(\mathbf{V} + \beta \alpha^2 \mathbf{P} + (1 - \beta) \alpha^4 \mathbf{Q} \right)^{-1} \mathbf{V} \mathbf{z} \quad (1)$$

where

- \mathbf{z} is the n -dimensional column vector of input data, e.g. the primary profile of n sampling points;
- \mathbf{w} is the column vector of output data, e.g. the waviness profile or smoothed profile;
- \mathbf{V} is the unity matrix in the case of the linear filter and the weighting matrix in the case of the robust filter;
- \mathbf{P} and \mathbf{Q} are the matrices for the discretized differentiation;
- β is the tension parameter (see also [4.2.3](#));
- α is the parameter (see [4.2.2](#)) depending on the smoothness, the nesting index (cut-off wavelength in the case of linear filters) of the spline.

[Formula \(1\)](#) is obtained by minimization of the objective (cost) function J as indicated in [Formula \(2\)](#):

$$\min_{\mathbf{w}} J \quad (2)$$

with the objective function defined in [Formula \(3\)](#):

$$J = (\mathbf{z} - \mathbf{w})^T \mathbf{V} (\mathbf{z} - \mathbf{w}) + \beta \alpha^2 \mathbf{w}^T \mathbf{P} \mathbf{w} + (1 - \beta) \alpha^4 \mathbf{w}^T \mathbf{Q} \mathbf{w} \quad (3)$$

where $\mathbf{Q} = \mathbf{P}^T \mathbf{P}$.

A sufficient condition of a minimum is $\nabla_{\mathbf{w}} J = 0$ leading to the filter equation in [Formula \(1\)](#).

NOTE 1 After extending the matrices of [Formula \(1\)](#) to tensors, the filter is also applicable to areal data^[11].

NOTE 2 Usually the objective function of smoothing splines is defined with a regularization parameter μ also fitted during the optimization process with an additional condition for the smoothness measured according to the deviations $z_i - s(x_i)$. Objective functions of the more common type of smoothing splines do not include non-zero tension $J = \sum_{i=1}^n (z_i - s(x_i))^2 + \mu \int_{x_1}^{x_n} \left(\frac{\partial}{\partial x} s(x) \right)^2 dx$ with $s(x)$ being the spline polynomials and the regularization parameter μ determining the degree of smoothing and hence following the data points vs approximating them.

4.2.2 Regularization parameter

The parameter μ specifies the regularization, i.e. the degree of smoothing. In the case of minimum tension, it holds $\mu = \alpha^4$ and is therefore related to the nesting index n_i , which is in the case of linear filtration equal to the cut-off wavelength λ_c as given in [Formula \(4\)](#):

$$\alpha = \frac{1}{2 \sin \left(\frac{\pi \Delta}{n_i} \right)} \quad (4)$$

where Δ is the sampling interval for uniformly sampled data and the average sampling interval as given in [Formula \(5\)](#):

$$\Delta = \frac{1}{n-1} \sum_{i=1}^{n-1} (x_{i+1} - x_i) \quad (5)$$

for data sampled non-uniformly at positions x_i with $i = 1, \dots, n-1$.

NOTE 1 [Formula \(4\)](#) is derived in Reference [\[12\]](#).

NOTE 2 For sampling intervals $\Delta \ll n_i$ the regularization parameter tends to infinity $\alpha^4 \rightarrow \infty$.

NOTE 3 For non-minimal tension the factor μ of the second order derivative term is also dependent on the tension parameter β : $\mu = (1 - \beta)\alpha^4$.

4.2.3 Tension parameter

The product $\beta\alpha^2$ is the tension factor with parameter β lying between 0 and 1. The parameter β controls the degree of subsequent topography curvatures, where curvature means a local property of a curve or a surface, which is defined at every point quantifying second-order deviations of a curve from a straight line or a surface from a plane.

Following curvatures closely means optimal shape retainment of the low-pass result, the output data w .

For $\beta = 0$ the characteristics of the transfer function conform to Formula (1) in ISO 16610-22, a minimum tension which is equivalent to the steepest slope of the transfer function and therefore a better shape retainment than for $\beta > 0$.

For $\beta = 0,625$ 242 the characteristics of the transfer function is similar to that of the Gaussian filter^[14] as specified in ISO 16610-21 and ISO 16610-61.

NOTE The shape retainment by the spline filter for $\beta = 0$ is global, while the shape retainment by the Gaussian regression with a parabolic regression ($p = 2$) is local.

4.2.4 Matrix V for linear cubic spline filter

Matrix V for linear filters is the $n \times n$ -dimensional unity matrix as given in [Formula \(6\)](#):

$$V = \begin{pmatrix} 1 & \dots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \dots & 1 \end{pmatrix} \quad (6)$$

4.2.5 Matrix V for robust cubic spline filter

Matrix V contains the weights suppressing specific phenomena in the input data. They are derived from Tukey's biweight influence function as given in [Formula \(7\)](#):

$$V^{(m)} = \begin{pmatrix} \delta_1 & \dots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \dots & \delta_n \end{pmatrix} \quad \text{with} \quad \delta_i = \begin{cases} \left(1 - \left(\frac{z_i - w_i^{(m)}}{c^{(m)}} \right)^2 \right)^2 & \text{for } |z_i - w_i^{(m)}| \leq c^{(m)} \\ 0 & \text{for } |z_i - w_i^{(m)}| > c^{(m)} \end{cases} \quad (7)$$

where

$$i = 1, \dots, n;$$

$$\mathbf{z} = (z_1, \dots, z_n)^T;$$

$$\mathbf{w}_i^{(m)} = (w_1^{(m)}, \dots, w_n^{(m)})^T;$$

superscript m denotes the iteration put into brackets, which is not to be confused with an exponent;

superscript T denotes transposed.

Furthermore, the parameter c is specified as given in ISO 16610-31:2016, Formula (8), and as shown in [Formula \(8\)](#):

$$c = a \operatorname{median}|z - \mathbf{w}| \quad \text{with} \quad a \cong 4,4478 \quad (8)$$

NOTE The exact value of a is obtained by the inverse error function erf^{-1} :

$$a = \frac{3}{\sqrt{2} \operatorname{erf}^{-1}(0,5)}$$

4.2.6 Termination of the iteration of robust estimation

The matrix \mathbf{V} containing weights δ_i being dependent on output data w_i starts with w obtained by linear non-robust filtration, i.e. $\mathbf{V}^{(0)}$ is the unity matrix. The iteration process terminates if the condition given in [Formula \(9\)](#) is reached:

$$\frac{|c^{(m+1)} - c^{(m)}|}{c^{(m)}} \leq 10^{-5} \quad \text{or} \quad m \geq 12 \quad (9)$$

4.2.7 Matrices of differentiation \mathbf{P} and \mathbf{Q}

4.2.7.1 General

A profile can be sampled at lateral positions x_i that are not necessarily equidistant. The lateral positions are strictly monotonically increasing, i.e. $x_i < x_{i+1}$.

The samplings intervals are denoted $\Delta_{i,j} = x_i - x_j$ and the quotient of the average sampling interval Δ and the distance between sampling positions x_i and x_j is denoted by $D_{i,j} = \frac{\Delta}{\Delta_{i,j}}$.

4.2.7.2 Differentiation matrix for first discretized derivative

For open profiles, matrix \mathbf{P} is tri-diagonal as shown in [Formula \(10\)](#):

$$\mathbf{P} = \begin{pmatrix} P_{1,1} & P_{1,2} & 0 & \cdots & & & \\ P_{2,1} & P_{2,2} & P_{2,3} & 0 & \cdots & & \\ 0 & P_{3,2} & P_{3,3} & P_{3,4} & 0 & \cdots & \\ & \ddots & \ddots & \ddots & \ddots & \ddots & \\ & & & & & & \end{pmatrix} \quad (10)$$

For rows $i = 2, \dots, n-1$ the main diagonal has the elements: $P_{i,i} = D_{i,i-1}^2 + D_{i+1,i}^2$.

The two off-diagonals have the elements $P_{i,i-1} = -D_{i,i-1}^2$ and $P_{i,i+1} = -D_{i+1,i}^2$.

The first two elements of the first row and the last two elements of the last row are as follows:

$$P_{1,1} = D_{1,2}^2 \quad \text{and} \quad P_{1,2} = -D_{1,2}^2 \quad \text{and} \quad P_{n,n-1} = -D_{n,n-1}^2 \quad \text{and} \quad P_{n,n} = D_{n,n-1}^2$$

For closed profiles the first row and the last row of the matrix differ, having additional non-zero entries at $P_{1,n}$ and at $P_{n,1}$ for the wrap around, i.e. the right neighbour of x_n is x_1 and the left neighbour of x_1 is x_n .

Then the first row has the following non-zeros entries:

$$P_{1,n} = -D_{1,n}^2 \text{ and } P_{1,1} = D_{1,n}^2 + D_{2,1}^2 \text{ and } P_{1,2} = -D_{2,1}^2$$

and the last row has the following entries:

$$P_{n,n-1} = -D_{n,n-1}^2 \text{ and } P_{n,n} = D_{n,n-1}^2 + D_{1,n}^2 \text{ and } P_{n,1} = -D_{1,n+1}^2$$

4.2.7.3 Differentiation matrix for second discretized derivative

For open profiles matrix Q is penta-diagonal as shown in [Formula \(11\)](#):

$$Q = \begin{pmatrix} Q_{1,1} & Q_{1,2} & Q_{1,3} & 0 & \dots \\ Q_{2,1} & Q_{2,2} & Q_{2,3} & Q_{2,4} & \ddots \\ Q_{3,1} & Q_{3,2} & Q_{3,3} & Q_{3,4} & Q_{3,5} \\ 0 & Q_{4,2} & Q_{4,3} & Q_{4,4} & Q_{4,5} & \ddots \\ & \ddots & \ddots & \ddots & \ddots & \ddots \end{pmatrix} \quad (11)$$

For rows $i=3, \dots, n-2$ the elements of the main diagonal are as follows:

$$Q_{i,i} = 4 \left(D_{i,i-1}^2 \left(D_{i,i-2}^2 + D_{i+1,i-1} D_{i+1,i} \right) + D_{i+1,i}^2 \left(D_{i+1,i-1} D_{i,i-1} + D_{i+2,i}^2 \right) \right)$$

The elements of the off-diagonal next to the main are as follows in the case of the upper:

$$Q_{i,i+1} = -4 D_{i+1,i} \left(D_{i+1,i} D_{i+1,i-1} D_{i,i-1} + D_{i+2,i}^2 \left(D_{i+2,i+1} + D_{i+1,i} \right) \right)$$

and in the case of the lower as follows:

$$Q_{i,i-1} = -4 D_{i,i-1} \left(D_{i+1,i} D_{i+1,i-1} D_{i,i-1} + D_{i,i-2}^2 \left(D_{i-1,i-2} + D_{i,i-1} \right) \right)$$

The elements of the second off-diagonals are in the case of the upper as follows:

$$Q_{i,i+2} = 4 D_{i+1,i} D_{i+2,i+1} D_{i+2,i}^2$$

and in the case of the lower as follows:

$$Q_{i,i-2} = 4 D_{i,i-2}^2 D_{i-1,i-2} D_{i,i-1}$$

For the first row and in the case of open profiles, the elements are as follows:

$$Q_{1,1} = 4 D_{2,1}^2 D_{3,1}^2 \text{ and } Q_{1,2} = -4 D_{2,1}^2 D_{3,2} D_{3,1} \text{ and } Q_{1,3} = 4 D_{3,2} D_{3,1}^2 D_{2,1}$$

For the second row and in the case of open profiles they are as follows:

$$Q_{2,1} = Q_{1,2} \text{ and } Q_{2,2} = 4 D_{3,2}^2 \left(D_{2,1}^2 + D_{4,2}^2 \right) \text{ and } Q_{2,3} = -4 D_{3,2}^2 \left(D_{2,1} D_{3,1} + D_{4,2} D_{4,3} \right)$$

$$Q_{2,3} = -4 D_{3,2} \left(D_{3,2} D_{3,1} D_{2,1} + D_{4,2}^2 \left(D_{4,3} + D_{3,2} \right) \right)$$

For closed profiles the first row has the following non-zero entries:

$$Q_{1,1} = 4 \left(D_{1,n}^2 \left(D_{1,n-1}^2 + D_{2,n} D_{2,1} \right) + D_{2,1}^2 \left(D_{2,n} D_{1,n} + D_{3,1}^2 \right) \right)$$

$$Q_{1,2} = -4 D_{2,1} \left(D_{2,1} D_{2,n} D_{1,n} + D_{3,1}^2 \left(D_{3,2} + D_{2,1} \right) \right)$$

$$Q_{1,n} = -4 D_{1,n} \left(D_{2,1} D_{2,n} D_{1,n} + D_{1,n-1}^2 \left(D_{n,n-1} + D_{1,n} \right) \right)$$

$$Q_{1,3} = 4 D_{2,1} D_{3,2} D_{3,1}^2 \text{ and } Q_{1,n-1} = 4 D_{1,n-1}^2 D_{n,n-1} D_{1,n}$$

The last row, in the case of closed profiles, has the following non-zero entries:

$$Q_{n,n} = 4 \left(D_{n,n-1}^2 \left(D_{n,n-2}^2 + D_{1,n-1} D_{1,n-1} \right) + D_{1,n}^2 \left(D_{1,n-1} D_{n,n-1} + D_{1,n}^2 \right) \right)$$

$$Q_{n1} = -4 D_{1,n} \left(D_{1,n} D_{1,n-1} D_{n,n-1} + D_{2,n}^2 \left(D_{2,1} + D_{1,n} \right) \right)$$

$$Q_{n,n-1} = -4 D_{n,n-1} \left(D_{1,n} D_{1,n-1} D_{n,n-1} + D_{n,n-2}^2 \left(D_{n-1,n-2} + D_{n,n-1} \right) \right)$$

$$Q_{n,2} = 4 D_{n+1,n} D_{2,1} D_{2,n}^2 \text{ and } Q_{n,n-2} = 4 D_{n,n-2}^2 D_{n-1,n-2} D_{n,n-1}$$

For closed profiles, the second row has the following non-zero entries:

$$Q_{2,2} = 4 \left(D_{2,1}^2 \left(D_{2,n}^2 + D_{3,1} D_{3,2} \right) + D_{3,2}^2 \left(D_{3,1} D_{2,1} + D_{4,2}^2 \right) \right)$$

$$Q_{2,3} = -4 D_{3,2} \left(D_{3,2} D_{3,1} D_{2,1} + D_{4,2}^2 \left(D_{4,3} + D_{3,2} \right) \right)$$

$$Q_{2,1} = -4 D_{2,1} \left(D_{3,2} D_{3,1} D_{2,1} + D_{2,n}^2 \left(D_{1,n} + D_{2,1} \right) \right)$$

$$Q_{2,4} = 4 D_{3,2} D_{4,3} D_{4,2}^2 \text{ and } Q_{2,n} = 4 D_{2,n}^2 D_{1,n} D_{2,1}$$

and the second-last row is as follows:

$$Q_{n-1,n-1} = 4 \left(D_{n-1,n-2}^2 \left(D_{n-1,n-3}^2 + D_{n,n-2} D_{n,n-2} \right) + D_{n,n-1}^2 \left(D_{n,n-2} D_{n-1,n-2} + D_{n,n-1}^2 \right) \right)$$

$$Q_{n-1,n} = -4 D_{n,n-1} \left(D_{n,n-1} D_{n,n-2} D_{n-1,n-2} + D_{1,n-1}^2 \left(D_{1,n} + D_{n,n-1} \right) \right)$$

$$Q_{n-1,n-2} = -4 D_{n-1,n-2} \left(D_{n,n-1} D_{n,n-2} D_{n-1,n-2} + D_{n-1,n-3}^2 \left(D_{n-2,n-3} + D_{n-1,n-2} \right) \right)$$

$$Q_{n-1,1} = 4 D_{n,n-1} D_{1,n} D_{1,n-1}^2 \text{ and } Q_{n-1,n-3} = 4 D_{n-1,n-3}^2 D_{n-2,n-3} D_{n-1,n-2}$$

4.3 Transmission characteristics

The transmission characteristics of the linear case, i.e. matrix \mathbf{V} , is a unity matrix as given in ISO 16610-22:2015, 4.3. The transmission characteristics of a robust filter do not exist, because of its nonlinearity.

4.4 Alternative robust spline filter

4.4.1 General

The weighting by the Tukey biweight function represents an M-estimator that causes a distribution of the residuals $z_i - w_i^{(m)}$ to be reshaped. The Tukey biweight influence function suppresses significantly large tails of a distribution or significant asymmetries. Hence the residuals contributing to filtration are almost Gaussian distributed. ISO 16610-30 allows alternative robust estimators that can be applied to spline filters in a generalized linear and nonlinear way. [13]

To retain the shape of profiles obtained on significantly curved surfaces within the waviness and to exclude this trend from roughness in ISO 16610-31, the default for the regression polynomial of the Gaussian regression is the parabola (i.e. order $p=2$). Retaining shape, i.e. passing curvature to the waviness profile, in the case of spline filters is obtained by minimizing the tension energy, which is equivalent to setting $\beta=0$.

When employing the least absolute deviation method, i.e. applying the L1-norm on the residuals, for robust estimation special care needs to be taken when defining the filter equation.

4.4.2 Objective function with L2-norm without tension energy for the linear filter equation

The filter equation, [Formula \(1\)](#), already represents the partial derivatives of the objective (cost) function J of the optimization problem^[8, 9] as given by [Formula \(12\)](#):

$$J = (\mathbf{z} - \mathbf{w})^T (\mathbf{z} - \mathbf{w}) + \alpha^4 \mathbf{w}^T \mathbf{Q} \mathbf{w} = \|\mathbf{z} - \mathbf{w}\|^2 + \alpha^4 \|\mathbf{P} \mathbf{w}\|^2 \quad (12)$$

For the case of minimum tension energy, i.e. $\beta=0$, and in the case of matrix \mathbf{V} being the unity matrix \mathbf{I} , which applies to the linear filter derived from the least mean square (LMS) method, use the L2-norm denoted with $\|\cdot\|^2$. The filter equation without tension energy reduces as given by [Formula \(13\)](#):

$$\mathbf{w} = (\mathbf{I} + \alpha^4 \mathbf{Q})^{-1} \mathbf{z} \quad (13)$$

where \mathbf{I} is the unit matrix.

4.4.3 Objective function with L1-norm without tension energy for robust filtration

For distributions of the residuals $r_i = z_i - w_i$ with extremely long tails and a very narrow kernel, i.e. for a kurtosis much greater than 3 (the kurtosis value 3 complies with a Gaussian distribution), assuming a Laplacian distribution rather than a Gaussian one is more appropriate. The Laplacian distribution has a kurtosis of 6. Assuming the residuals $z_i - w_i$ to follow a Laplacian distribution with zero mean, the target function is given in [Formula \(14\)](#):

$$J = \left(\frac{\pi}{2} \frac{1}{n} \|\mathbf{z} - \mathbf{w}^{(m-1)}\| \right) \|\mathbf{z} - \mathbf{w}\| + \alpha^4 \|\mathbf{P} \mathbf{w}\|^2 \quad (14)$$

where $\|\cdot\|$ denotes the L1-norm.

The factor $\frac{\pi}{2} \frac{1}{n} \|\mathbf{z} - \mathbf{w}^{(m-1)}\|$ provides for an appropriate scaling carrying the dimension of a length,^[14] with n being the number of sampling points and m the iteration step. The sum of absolute values of the residuals of the previous iteration is used to estimate this factor.

Dividing the objective function by c for further processing, the optimization problem is written in a form suitable for the split-Bregman algorithm. The optimization problem is expressed by [Formula \(15\)](#):

$$\min_{\mathbf{w}, \mathbf{r}} \{ \|\mathbf{r}\| + \mu \|\mathbf{P} \mathbf{w}\|^2 \} \quad (15)$$

where $\mathbf{r} = \mathbf{z} - \mathbf{w}$ and the regularization parameter μ is given by [Formula \(16\)](#):

$$\mu = \frac{\alpha^4}{\frac{\pi}{2} \frac{1}{n} \|\mathbf{z} - \mathbf{w}^{(m-1)}\|} \quad (16)$$

which is equivalent to the optimization problem as given by [Formula \(17\)](#):

$$\min_{\mathbf{w}, \mathbf{r}} \{ \|\mathbf{r}\| + \mu \|\mathbf{P} \mathbf{w}\|^2 + \lambda \|\mathbf{z} - \mathbf{w}\|^2 \} \quad (17)$$

where λ is Lagrange multipliers carrying the dimension of an inverse length.

The Lagrange multipliers are proportional to $\frac{1}{\frac{\pi}{2} \frac{1}{n} \|\mathbf{z} - \mathbf{w}^{(m-1)}\|}$ (see Reference [\[15\]](#)).

5 Filter designation

The linear spline filter, i.e. the filter with matrix \mathbf{V} being the unity matrix, is designated:

FPLS

and the robust spline filter, the filter with matrix \mathbf{V} being a weighting matrix, as given in [Formula \(7\)](#), is designated:

FPRS

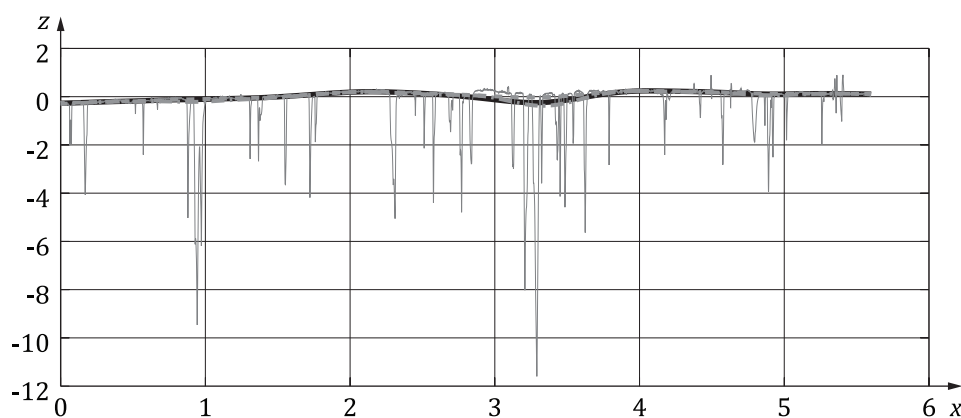
See also ISO 16610-1.

Annex A (informative)

Example of spline filter applied to plateau structured profile

Typical use cases for robust filters include determining material ratio parameters of measurement data on plateau structured surfaces, i.e. profiles with extremely skewed amplitude distributions.

[Figure A.1](#) displays a profile of a sintered surface filtered with a nesting index of $n_i = 0,8$ mm. The split-Bregman algorithm for L1-norm optimization complies with one or two iterations when employing M-estimation with the Tukey biweight function as weighting function depending on the residuals to suppress long tails.



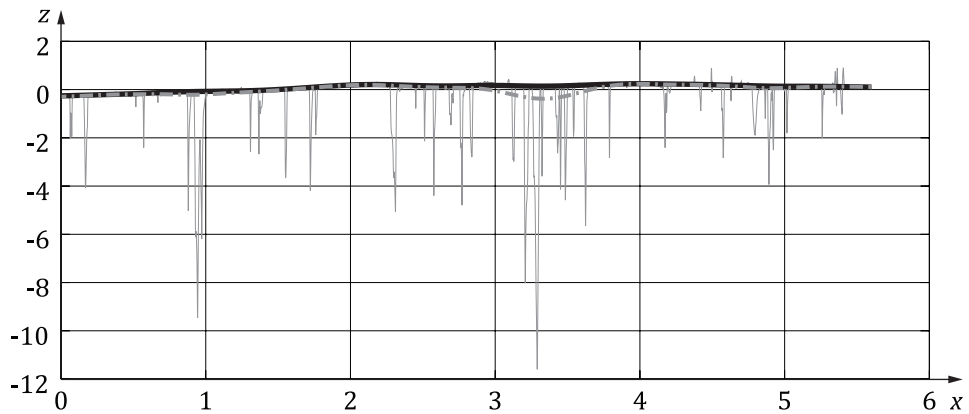
Key

z	height values of the profile, in μm
x	positions along the lateral scan axis, in mm
-----	Tukey 1 iteration
.....	Tukey 2 iteration
————	L1-norm

NOTE It is obtained by applying the M-estimator approach with the Tukey biweight function with only 1 and 2 iterative steps in comparison with the result of the L1-norm obtained by the Bregmen split procedure, with a nesting index of $n_i = 0,8$ mm and a tension parameter of $\beta = 0$.

Figure A.1 — Profile of sintered surface and its spline filtered waviness profiles

[Figure A.2](#) illustrates the effect of iteratively applying the M-estimator approach until it converges to a stable waviness curve no longer following the deep grooves. It shows the difference between the waviness profile obtained by applying the M-estimator approach with the Tukey biweight function with only 1 iteration and with as many iterative steps as to guarantee one stable result, with a nesting index of $n_i = 0,8$ mm and a tension parameter of $\beta = 0$.

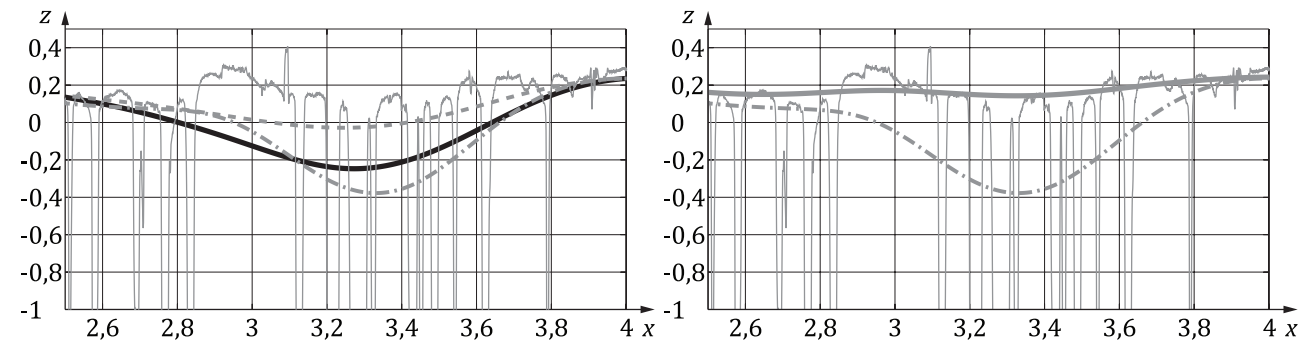


Key

- z height values of the profile, in μm
- x positions along the lateral scan axis, in mm
- Tukey 21 iterations
- - - - - Tukey 1 iteration

Figure A.2 — Profile of [Figure A.1](#)

The feature of the profile that lies between 3 mm and 4 mm clearly reveals the idea of the robust filtration to obtain a waviness that represents the surface as a plateau. The waviness is a straight bridge across all the grooves. [Figure A.3](#) therefore depicts this detail as an example. It shows the idea of a waviness profile to represent the plateau of a surface with grooves, which can be interpreted as bridges crossing the grooves.



Key

- z height values of the profile, in μm
- x positions along the lateral scan axis, in mm
- - - - - Tukey 1 iteration
- Tukey 2 iterations
- Tukey 21 iterations
- Tukey 1 iteration

Figure A.3 — Detail of a small interval of the profile of [Figures A.1](#) and [A.2](#)

Annex B (informative)

Relationship to the filtration matrix model

B.1 General

For full details about the filtration matrix model, see ISO 16610-1.

B.2 Position in the filtration matrix model

This document influences particular filters in the column “Profile filters, Robust” in [Table B.1](#).

Table B.1 — Relationship to the filtration matrix model

General	Filters: ISO 16610 series					
	Part 1					
Fundamental	Profile filters			Areal filters		
	ISO 16610-11 ^a			ISO 16610-12 ^a		
	Linear	Robust	Morphological	Linear	Robust	Morphological
Basic concepts	Part 20	Part 30	Part 40	Part 60	Part 70	Part 80
Particular filters	Parts 21 to 25	Parts 31 to 35	Parts 41 to 45	Parts 61 to 65	Parts 71 to 75	Parts 81 to 85
How to filter	Parts 26 to 28	Parts 36 to 38	Parts 46 to 48	Parts 66 to 68	Parts 76 to 78	Parts 86 to 88
Multiresolution	Part 29	Part 39	Part 49	Part 69	Part 79	Part 89

^a At present included in ISO 16610-1.

Annex C (informative)

Relationship to the GPS matrix model

C.1 General

The ISO GPS matrix model given in ISO 14638 gives an overview of the ISO GPS system, of which this document is a part.

The fundamental rules of ISO GPS given in ISO 8015 apply to this document and the default decision rules given in ISO 14253-1 apply to specifications made in accordance with this document, unless otherwise indicated.

C.2 Information about this document and its use

This document is a Technical Report which develops the terminology and concepts for spline filters.

C.3 Position in the GPS matrix model

This document is a general ISO GPS document which influences chain link C of the chains of standards on feature properties in the GPS matrix model, as shown in [Table C.1](#). The rules and principles given in this document apply to all segments of the ISO GPS matrix which are indicated with a filled dot (•).

Table C.1 — ISO GPS Standards matrix model

	Chain links						
	A	B	C	D	E	F	G
	Symbols and indications	Feature requirements	Feature properties	Conformity and non-conformity	Measurement	Measurement equipment	Calibration
Size			•				
Distance			•				
Form			•				
Orientation			•				
Location			•				
Run-out			•				
Profile surface texture			•				
Areal surface texture			•				
Surface imperfections			•				

C.4 Related International Standards

The related International Standards are those of the chains of standards indicated in [Table C.1](#).

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- [1] ISO 8015, *Geometrical product specifications (GPS) — Fundamentals — Concepts, principles and rules*
- [2] ISO 14253-1, *Geometrical product specifications (GPS) — Inspection by measurement of workpieces and measuring equipment — Part 1: Decision rules for verifying conformity or nonconformity with specifications*
- [3] ISO 14638, *Geometrical product specifications (GPS) — Matrix model*
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