***भारतीय मानक*  IS 228 (Part 1) : 2024**

***Indian Standard***

**इस्पात के रासायनिक विश्लेषण की**

**पद्धतियाँ**

**भाग 1 आयतनात्मक पद्धति द्वारा कुल कार्बन का निर्धारण (कार्बन 0.05 से 2.50 प्रतिशत के लिए**

*(*चौथा *पुनरीक्षण)*

**Methods for Chemical Analysis of Steels**

**Part 1 Determination of Carbon by Volumetric Method**

**(For Carbon 0.05 To 2.50 Percent)**

*( Fourth Revision )*

ICS 77.080.20

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भारतीय मानक ब्यूरो

BUREAU OF INDIAN STANDARDS

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**October2024 Price Group**

Methods of Chemical Analysis of Metals Sectional Committee, MTD 34

FOREWORD

This Indian Standard (Part 1) (Fourth Revision) was adopted by the Bureau of Indian Standards after the draft finalized by the Methods of Chemical analysis of Metals Sectional Committee had been approved by the Metallurgical Engineering Division Council.

This standard was first published in 1952 and subsequently revised in 1959, 1972 and 1987. This revision has been brought out to bring the standard in the latest style and format of the Indian Standards.

This standard covers chemical analysis of both plain carbon and low alloy steels, along with pig iron and cast iron.

This part covers the methods for determination of carbon. The other parts of this series are:

|  |  |
| --- | --- |
| Part 2 | Determination of manganese in plain carbon and low alloy steels by arsenite method |
| Part 3 | Determination of phosphorus by alkalimetric method |
| Part 4 | Determination of total carbon by gravimetric method (for carbon greater than or equal to 0.1 percent) |
| Part 5 | Determination of nickel by dimethyl glyoxime (gravimetric) method (for nickel greater than or equal to 0.1 percent) |
| Part 6 | Determination of chromium by persulphate oxidation method (for chromium ≥ 0.1 percent ) |
| Part 7 | Determination of molybdenum by alpha benzoinoxime method (for molybdenum 1 percent and not containing tungsten) |
| Part 8 | Determination of silicon by gravimetric method (for silicon 0.05 to 5.00 percent) |
| Part 9 | Determination of sulphur in plain carbon steels by evolution method (for sulphur 0.01 to 0.25 percent) |
| Part 10 | Determination of molybdenum by thiocyanate (photometric) method in low and high alloy steels (for molybdenum 0.01 to 1.5 percent) |
| Part 11 | Determination of silicon by reduced molybdosilicate spectrophotometric method in carbon steels and low alloy steels (for silicon 0.01 to 0.05 percent) |
| Part 12 | Determination of manganese by periodate spectrophotometric method in plain carbon, low alloy and high alloy steels (for manganese 0.01 to 5.0 percent) |
| Part 13 | Determination of arsenic |
| Part 14 | Determination of carbon by thermal conductivity method (for carbon 0.005 to 2.000 percent) |
| Part 15 | Determination of copper by thiosulphate iodide method (for copper 0.05 to 5 percent) |
| Part 16 | Determination of tungsten by spectrophotometric method (for tungsten 0.1 to 2 percent) |
| Part 17 | Determination of nitrogen by thermal conductivity method |
| Part 18 | Determination of oxygen by instrumental method (for oxygen 0.001 to 0.100 0 percent) |
| Part 19 | Determination of nitrogen by steam distillation |
| Part 20 | Determination of carbon and sulphur by infrared absorption method |
| Part 21 | Determination of copper by spectrometric method (for copper 0.02 to 0.5 percent) |
| Part 22 | Determination of total hydrogen in steel by thermal conductivity method (hydrogen 0.1 ppm to 50 ppm) |
| Part 23 | Determination of total nitrogen in steel by optical emission spectrometer (nitrogen 0.002 to 1.0 percent) |
| Part 24 | Determination of nitrogen in steel by inert gas fusion – Thermal conductivity method (nitrogen 0.001 to 0.2 percent). |

The composition of the Committee responsible for the formulation of this standard is given in Annex A.

In reporting the results of a test or analysis made in accordance with this standard, if the final value, observed or calculated, is to be rounded off, it shall be done in accordance with IS 2 : 2022 ‘Rules for rounding off numerical values (*second revision*)’.

*Indian Standard*

METHODS FOR CHEMICAL ANALYSIS OF STEELS

PART 1 DETERMINATION OF CARBON BY VOLUMETRIC METHOD

(FOR CARBON 0.05 TO 2.50 PERCENT)

*( Fourth Revision )*

**1 Scope**

This standard (Part 1) covers volumetric method for determination of carbon in the range 0.05 to 2.50 percent in plain carbon, low alloy and high alloys steels.

**2 REFERENCES**

The following standards contain provisions, which through reference in this text, constitute provisions of this standard. At the time of publication the editions indicated were valid. All standards are subject to revision and parties to agreements based on this standard are encouraged to investigate the possibility of applying the most recent editions of the standards indicated below:

|  |  |
| --- | --- |
| *IS No.* | *Title* |
| IS 264 : 2005 | Nitric acid — Specification (*third revision*) |
| IS 265 : 2021 | Hydrochloric acid — Specification (*fifth revision*) |
| IS 6226 (Part 1) : 1994 | Recommendations for apparatus for chemicals analysis of metals: Part 1 Apparatus for determination of carbon by direct combustion (*first revision*) |

**3 Sampling**

The sample shall be drawn as prescribed in the relevant Indian Standard. (The sample is cleaned with organic solvent like ether or acetone, dried in an air oven at 100 ºC ± 5 ºC before use).

**4 Apparatus**

The apparatus recommended in IS 6226 (Part 1) may be used.

**5 DETERMINATION OF CARBON BY VOLUMETRIC METHOD**

**5.1 Outline of the Method**

The sample is burnt in a current of pure oxygen in presence of a suitable flux. Combustion of the sample in a stream of oxygen, thus converts all the carbon present to carbon dioxide. After removal of sulphurous gases by suitable absorbents, the carbon dioxide gas is collected in a specially jacketed burette along with excess of oxygen. The carbon dioxide is then absorbed in alkali. On passing the excess oxygen back to the burette, the contraction in volume is read against a scale, calibrated directly to the percentage of carbon.

**5.2 Procedure**

**5.2.1** Before use the apparatus should be tested for satisfactory working against standard steel of appropriate values of carbon.

**5.2.2** *For Plain Carbon Steel*

Take one gram of an accurately weighed and clean sample free from extraneous carbon in the form of small drillings or shavings in a porcelain boat which can withstand a temperature of 1 150 °C without breaking or cracking.

**5.2.2.1** Introduce the boat into the hot combustion tube in the furnace kept at 1 000 ºC to 1 100 ºC.

**5.2.3** *For Low Alloy and High Alloy Steels*

Take one gram of an accurately weighed and clean sample free from extraneous carbon in the form of small drillings or shavings in a porcelain boat, which can stand a temperature of 1 250 ºC without breaking and cracking. Spread 0.5 g of pure tin granules over the sample. In case of high alloy steel mix the sample with 0.5 g of pure iron (99.99 percent) filings also. Introduce the boat into the hot combustion tube in the furnace, kept between 1 150 ºC to 1 250 °C.

**5.2.4** Close the furnace inlet with a rubber stopper, allow the sample to heat for one to one and a half minute. Regulate the flow of oxygen to 300 ml to 400 ml per minute into the furnace and establish connection with the burette, which has been previously filled with acidulated water/brine water coloured with methyl red, so that the liquid level in the bulbed portion of the gas burette does not fall rapidly. After a minute or so the level of water in the burette begins to fall more rapidly, though the same rate of oxygen is maintained, indicating completion of combustion.

**5.2.5** Take readings, when the level reaches near the zero graduation mark after closing the bend way stopcock and equalizing the levels of the burette and the connected levelling bottle. Pass the collected and measured gas twice into the absorbing bulb, till constant reading is obtained, Record the burette reading. On the basis of one gram of sample taken for analysis, the burette is graduated to measure directly the percentage of carbon.

**5.2.5.1** Examine the combustion boat for complete fusion of the sample, if not thoroughly fused, repeat the determination with a fresh sample.

**5.3 Blank**

Run a blank experiment on the same quantity of accelerators used, without any sample and make the appropriate corrections.

**5.4 Calculation**

Carbon, percent *=* (*A* − *B*)× *F*

where

*A* = burette reading after absorption of carbon dioxide in caustic potash with one gram of sample,

*B* = burette reading for the blank experiment, and

*F* = Correction teeter for temperature and pressure (*see* Table 1).

**5.5** **Reproducibility**

± 0·01 percent up to 1.50 percent carbon, and

± 0·02 percent above 1.50 percent carbon.

**Table 1 Correction Factors**

(*Clause* 5.4)

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| **Pressure,**  mm Hg  **Tempera-**  **ture**, ºC | 700 | 702 | 704 | 706 | 708 | 710 | 712 | 714 | 716 | 718 | 720 | 722 | 724 | 726 | 728 | 730 | 732 | 734 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 15 | 0.924 | 0.927 | 0.929 | 0.932 | 0.935 | 0.937 | 0.940 | 0.943 | 0.945 | 0.948 | 0.951 | 0.954 | 0.956 | 0.959 | 0.962 | 0.964 | 0.967 | 0.970 |
| 16 | 0.920 | 0.922 | 0.925 | 0.928 | 0.930 | 0.930 | 0.936 | 0.938 | 0.941 | 0.944 | 0.946 | 0.949 | 0.952 | 0.954 | 0.957 | 0.960 | 0.962 | 0.965 |
| 17 | 0.915 | 0.918 | 0.921 | 0.923 | 0.926 | 0.929 | 0.931 | 0.934 | 0.937 | 0.939 | 0.942 | 0.945 | 0.947 | 0.950 | 0.953 | 0.955 | 0.958 | 0.961 |
| 18 | 0.911 | 0.914 | 0.916 | 0.919 | 0.922 | 0.924 | 0.927 | 0.929 | 0.932 | 0.935 | 0.937 | 0.940 | 0.943 | 0.945 | 0.948 | 0.951 | 0.953 | 0.956 |
| 19 | 0.906 | 0.909 | 0.912 | 0.914 | 0.917 | 0.920 | 0.922 | 0.925 | 0.928 | 0.930 | 0.933 | 0.936 | 0.938 | 0.941 | 0.944 | 0.946 | 0.949 | 0.952 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 20 | 0.902 | 0.904 | 0.907 | 0.910 | 0.912 | 0.915 | 0.918 | 0.920 | 0.923 | 0.926 | 0.928 | 0.931 | 0.934 | 0.936 | 0.939 | 0.942 | 0.944 | 0.947 |
| 21 | 0.897 | 0.900 | 0.903 | 0.905 | 0.908 | 0.910 | 0.913 | 0.916 | 0.918 | 0.921 | 0.924 | 0.926 | 0.929 | 0.932 | 0.934 | 0.937 | 0.940 | 0.942 |
| 22 | 0.893 | 0.895 | 0.898 | 0.901 | 0.903 | 0.906 | 0.908 | 0.911 | 0.914 | 0.916 | 0.919 | 0.922 | 0.924 | 0.927 | 0.930 | 0.932 | 0.935 | 0.937 |
| 23 | 0.888 | 0.891 | 0.893 | 0.896 | 0.899 | 0.901 | 0.904 | 0.906 | 0.909 | 0.912 | 0.914 | 0.917 | 0.912 | 0.922 | 0.925 | 0.927 | 0.930 | 0.933 |
| 24 | 0.883 | 0.886 | 0.889 | 0.891 | 0.894 | 0.896 | 0.899 | 0.902 | 0.904 | 0.907 | 0.910 | 0.912 | 0.915 | 0.917 | 0.920 | 0.922 | 0.925 | 0.928 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | 0.879 | 0.881 | 0.884 | 0.886 | 0.889 | 0.892 | 0.894 | 0.897 | 0.900 | 0.902 | 0.905 | 0.907 | 0.910 | 0.912 | 0.915 | 0.918 | 0.920 | 0.923 |
| 26 | 0.874 | 0.876 | 0.879 | 0.882 | 0.884 | 0.887 | 0.889 | 0.892 | 0.894 | 0.897 | 0.900 | 0.902 | 0.905 | 0.908 | 0.910 | 0.913 | 0.915 | 0.918 |
| 27 | 0.869 | 0.872 | 0.874 | 0.877 | 0.879 | 0.882 | 0.884 | 0.887 | 0.890 | 0.892 | 0.895 | 0.897 | 0.900 | 0.902 | 0.905 | 0.908 | 0.910 | 0.913 |
| 28 | 0.864 | 0.867 | 0.869 | 0.872 | 0.874 | 0.877 | 0.879 | 0.882 | 0.885 | 0.887 | 0.890 | 0.892 | 0.895 | 0.898 | 0.900 | 0.903 | 0.905 | 0.908 |
| 29 | 0.859 | 0.862 | 0.864 | 0.867 | 0.869 | 0.872 | 0.874 | 0.877 | 0.880 | 0.882 | 0.885 | 0.887 | 0.890 | 0.892 | 0.895 | 0.897 | 0.900 | 0.903 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | 0.854 | 0.856 | 0.859 | 0.862 | 0.864 | 0.867 | 0.869 | 0.872 | 0.874 | 0.877 | 0.879 | 0.882 | 0.884 | 0.887 | 0.890 | 0.892 | 0.895 | 0.897 |
| 31 | 0.849 | 0.851 | 0.854 | 0.856 | 0.859 | 0.861 | 0.864 | 0.866 | 0.869 | 0.872 | 0.874 | 0.877 | 0.879 | 0.882 | 0.884 | 0.887 | 0.889 | 0.892 |
| 32 | 0.843 | 0.846 | 0.848 | 0.851 | 0.854 | 0.856 | 0.859 | 0.861 | 0.864 | 0.866 | 0.869 | 0.871 | 0.874 | 0.876 | 0.879 | 0.882 | 0.884 | 0.886 |
| 33 | 0.838 | 0.840 | 0.843 | 0.846 | 0.848 | 0.851 | 0.853 | 0.856 | 0.858 | 0.861 | 0.863 | 0.866 | 0.868 | 0.871 | 0.873 | 0.876 | 0.878 | 0.881 |
| 34 | 0.833 | 0.835 | 0.838 | 0.840 | 0.843 | 0.845 | 0.848 | 0.850 | 0.853 | 0.855 | 0.858 | 0.860 | 0.863 | 0.865 | 0.868 | 0.870 | 0.873 | 0.875 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 35 | 0.827 | 0.830 | 0.832 | 0.834 | 0.837 | 0.840 | 0.842 | 0.845 | 0.847 | 0.850 | 0.852 | 0.855 | 0.857 | 0.860 | 0.862 | 0.865 | 0.867 | 0.870 |
| 36 | 0.821 | 0.824 | 0.826 | 0.829 | 0.831 | 0.834 | 0.836 | 0.839 | 0.841 | 0.844 | 0.846 | 0.849 | 0.851 | 0.854 | 0.856 | 0.859 | 0.861 | 0.864 |
| 37 | 0.816 | 0.818 | 0.820 | 0.823 | 0.826 | 0.828 | 0.830 | 0.833 | 0.836 | 0.838 | 0.840 | 0.843 | 0.846 | 0.848 | 0.850 | 0.853 | 0.856 | 0.858 |
| 38 | 0.810 | 0.812 | 0.815 | 0.817 | 0.820 | 0.822 | 0.825 | 0.827 | 0.830 | 0.832 | 0.834 | 0.837 | 0.840 | 0.842 | 0.844 | 0.847 | 0.850 | 0.852 |
| 39 | 0.804 | 0.806 | 0.809 | 0.811 | 0.814 | 0.816 | 0.818 | 0.821 | 0.824 | 0.826 | 0.828 | 0.831 | 0.833 | 0.836 | 0.838 | 0.841 | 0.843 | 0.846 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | 0.798 | 0.800 | 0.802 | 0.805 | 0.807 | 0.810 | 0.812 | 0.815 | 0.817 | 0.820 | 0.822 | 0.825 | 0.827 | 0.830 | 0.832 | 0.835 | 0.837 | 0.840 |
| 41 | 0.791 | 0.794 | 0.796 | 0.799 | 0.801 | 0.804 | 0.806 | 0.808 | 0.811 | 0.813 | 0.816 | 0.818 | 0.821 | 0.823 | 0.826 | 0.828 | 0.831 | 0.833 |
| 42 | 0.785 | 0.787 | 0.790 | 0.792 | 0.795 | 0.797 | 0.800 | 0.802 | 0.804 | 0.807 | 0.809 | 0.812 | 0.814 | 0.817 | 0.819 | 0.822 | 0.824 | 0.827 |
| 43 | 0.778 | 0.781 | 0.783 | 0.786 | 0.788 | 0.791 | 0.793 | 0.796 | 0.798 | 0.800 | 0.803 | 0.805 | 0.808 | 0.810 | 0.813 | 0.815 | 0.818 | 0.820 |
| 44 | 0.772 | 0.774 | 0.776 | 0.779 | 0.781 | 0.784 | 0.786 | 0.789 | 0.791 | 0.794 | 0.796 | 0.798 | 0.801 | 0.803 | 0.806 | 0.808 | 0.811 | 0.813 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 45 | 0.765 | 0.761 | 0.770 | 0.772 | 0.775 | 0.777 | 0.779 | 0.782 | 0.784 | 0.787 | 0.789 | 0.792 | 0.794 | 0.796 | 0.799 | 0.801 | 0.804 | 0.806 |

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| **Pressure,**  mm Hg  **Tempera-**  **ture**, ºC | 736 | 738 | 740 | 742 | 744 | 746 | 748 | 750 | 752 | 754 | 756 | 758 | 760 | 762 | 764 | 766 | 768 | 770 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 15 | 0.972 | 0.975 | 0.978 | 0.980 | 0.983 | 0.986 | 0.988 | 0.991 | 0.994 | 0.996 | 0.999 | 1.002 | 1.005 | 1.007 | 1.010 | 1.013 | 1.015 | 1.018 |
| 16 | 0.968 | 0.970 | 0.973 | 0.976 | 0.978 | 0.981 | 0.984 | 0.987 | 0.989 | 0.992 | 0.995 | 0.997 | 1.000 | 1.003 | 1.005 | 1.008 | 1.011 | 1.013 |
| 17 | 0.963 | 0.966 | 0.969 | 0.971 | 0.974 | 0.977 | 0.979 | 0.982 | 0.985 | 0.987 | 0.990 | 0.993 | 0.995 | 0.998 | 1.001 | 1.003 | 1.006 | 1.009 |
| 18 | 0.959 | 0.961 | 0.964 | 0.967 | 0.969 | 0.972 | 0.975 | 0.977 | 0.980 | 0.983 | 0.985 | 0.988 | 0.991 | 0.993 | 0.996 | 0.999 | 1.001 | 1.004 |
| 19 | 0.954 | 0.957 | 0.959 | 0.962 | 0.965 | 0.967 | 0.970 | 0.973 | 0.975 | 0.978 | 0.981 | 0.983 | 0.986 | 0.989 | 0.991 | 0.994 | 0.996 | 0.999 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 20 | 0.950 | 0.952 | 0.955 | 0.957 | 0.960 | 0.963 | 0.965 | 0.968 | 0.971 | 0.973 | 0.976 | 0.978 | 0.981 | 0.984 | 0.986 | 0.989 | 0.992 | 0.994 |
| 21 | 0.945 | 0.947 | 0.950 | 0.953 | 0.955 | 0.958 | 0.961 | 0.963 | 0.966 | 0.968 | 0.971 | 0.974 | 0.976 | 0.979 | 0.982 | 0.984 | 0.987 | 0.990 |
| 22 | 0.940 | 0.943 | 0.945 | 0.948 | 0.950 | 0.953 | 0.956 | 0.958 | 0.961 | 0.964 | 0.966 | 0.969 | 0.972 | 0.974 | 0.977 | 0 979 | 0.982 | 0.985 |
| 23 | 0.935 | 0.938 | 0.940 | 0.943 | 0.946 | 0.948 | 0.951 | 0.954 | 0.956 | 0.959 | 0.961 | 0.964 | 0.967 | 0.969 | 0.972 | 0.974 | 0.977 | 0.980 |
| 24 | 0.930 | 0.933 | 0.936 | 0.938 | 0.941 | 0.943 | 0.946 | 0.949 | 0.951 | 0.954 | 0.956 | 0.959 | 0.962 | 0.964 | 0.967 | 0.967 | 0.972 | 0.975 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | 0.925 | 0.928 | 0.931 | 0.933 | 0.936 | 0.938 | 0.941 | 0.944 | 0.946 | 0.949 | 0.951 | 0.954 | 0.957 | 0.959 | 0.962 | 0.964 | 0.967 | 0.970 |
| 26 | 0.920 | 0.923 | 0.926 | 0.928 | 0.931 | 0.933 | 0.936 | 0.939 | 0.941 | 0.944 | 0.946 | 0.949 | 0.952 | 0.954 | 0.957 | 0.959 | 0.962 | 0.964 |
| 27 | 0.915 | 0.918 | 0.921 | 0.923 | 0.926 | 0.928 | 0.931 | 0.934 | 0.936 | 0.939 | 0.941 | 0.944 | 0.946 | 0.949 | 0.952 | 0.954 | 0.957 | 0.959 |
| 28 | 0.910 | 0.913 | 0.916 | 0.918 | 0.921 | 0.923 | 0.926 | 0.928 | 0.931 | 0.934 | 0.936 | 0.939 | 0.941 | 0.944 | 0.946 | 0.949 | 0.952 | 0.954 |
| 29 | 0.905 | 0.908 | 0.910 | 0.913 | 0.915 | 0.918 | 0.920 | 0.923 | 0.926 | 0.928 | 0.931 | 0.933 | 0.936 | 0.938 | 0.941 | 0.944 | 0.946 | 0.949 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | 0.900 | 0.902 | 0.905 | 0.908 | 0.910 | 0.913 | 0.915 | 0.918 | 0.920 | 0.923 | 0.925 | 0.928 | 0.930 | 0.933 | 0.936 | 0.938 | 0.941 | 0.943 |
| 31 | 0.894 | 0.897 | 0.900 | 0.902 | 0.905 | 0.907 | 0.910 | 0.912 | 0.915 | 0.917 | 0.920 | 0.922 | 0.925 | 0.928 | 0.930 | 0.933 | 0.935 | 0.938 |
| 32 | 0.889 | 0.892 | 0.894 | 0.897 | 0.899 | 0.902 | 0.904 | 0.907 | 0.909 | 0.912 | 0.914 | 0.917 | 0.920 | 0.922 | 0.925 | 0.927 | 0.930 | 0.932 |
| 33 | 0.884 | 0.886 | 0.889 | 0.891 | 0.894 | 0.896 | 0.899 | 0.901 | 0.904 | 0.906 | 0.909 | 0.911 | 0.914 | 0.916 | 0.919 | 0.922 | 0.924 | 0.927 |
| 34 | 0.878 | 0.880 | 0.883 | 0.886 | 0.888 | 0.891 | 0.893 | 0.896 | 0.898 | 0.901 | 0.903 | 0.906 | 0.908 | 0.911 | 0.913 | 0.916 | 0.918 | 0.921 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 35 | 0.872 | 0.875 | 0.877 | 0.880 | 0.882 | 0.885 | 0.887 | 0.890 | 0.892 | 0.895 | 0.897 | 0.900 | 0.902 | 0.905 | 0.907 | 0.910 | 0.912 | 0.915 |
| 36 | 0.866 | 0.869 | 0.871 | 0.874 | 0.876 | 0.879 | 0.882 | 0.884 | 0.886 | 0.889 | 0.892 | 0.894 | 0.896 | 0.899 | 0.902 | 0.904 | 0.906 | 0.909 |
| 37 | 0.860 | 0.863 | 0.866 | 0.868 | 0.870 | 0.873 | 0.876 | 0.878 | 0.880 | 0.883 | 0.886 | 0.888 | 0.890 | 0.893 | 0.896 | 0.898 | 0.900 | 0.903 |
| 38 | 0.854 | 0.857 | 0.859 | 0.862 | 0.864 | 0.867 | 0.869 | 0.872 | 0.874 | 0.877 | 0.879 | 0.882 | 0.884 | 0.887 | 0.889 | 0.892 | 0.894 | 0.897 |
| 39 | 0.848 | 0.851 | 0.853 | 0.856 | 0.858 | 0.861 | 0.863 | 0.866 | 0.868 | 0.871 | 0.873 | 0.876 | 0.878 | 0.881 | 0.883 | 0.886 | 0.888 | 0.890 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | 0.842 | 0.844 | 0.847 | 0.850 | 0.852 | 0.854 | 0.857 | 0.859 | 0.862 | 0.864 | 0.867 | 0.869 | 0.872 | 0.874 | 0.877 | 0.879 | 0.882 | 0.884 |
| 41 | 0.836 | 0.838 | 0.841 | 0.843 | 0.846 | 0.848 | 0.850 | 0.853 | 0.855 | 0.858 | 0.860 | 0.863 | 0.865 | 0.868 | 0.870 | 0.873 | 0.875 | 0.878 |
| 42 | 0.829 | 0.832 | 0.834 | 0.836 | 0.839 | 0.841 | 0.844 | 0.846 | 0.849 | 0.851 | 0.854 | 0.856 | 0.859 | 0.861 | 0.864 | 0.866 | 0.868 | 0.870 |
| 43 | 0.822 | 0.825 | 0.827 | 0.830 | 0.832 | 0.835 | 0.837 | 0.840 | 0.842 | 0.844 | 0.847 | 0.849 | 0.852 | 0.854 | 0.857 | 0.859 | 0.862 | 0.864 |
| 44 | 0.816 | 0.818 | 0.820 | 0.823 | 0.825 | 0 828 | 0.830 | 0.833 | 0.835 | 0.838 | 0.840 | 0.842 | 0.845 | 0.847 | 0.850 | 0.852 | 0.855 | 0.857 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 45 | 0.809 | 0.811 | 0.814 | 0.816 | 0.818 | 0.821 | 0.823 | 0.826 | 0.828 | 0.830 | 0.833 | 0.835 | 0.838 | 0.840 | 0.843 | 0.845 | 0.848 | 0.850 |

**ANNEX A**

(*Foreword*)

**COMMITTEE COMPOSITION**

Methods of Chemical Analysis of Metals Sectional Committee, MTD 34

| *Organization* |  | *Representative(s)* |
| --- | --- | --- |
| CSIR - National Metallurgical Laboratory, Jamshedpur |  | Dr Sanchita Chakravarty **(*Chairperson*)** |
| Arcelor Mittal Nippon Steel, Mumbai |  | Shri Manoj Gupta |
| Shri Kirit Tailor (*Alternate*) |
| Bhabha Atomic Research Centre, Mumbai |  | Ms Sanjukta A. Kumar |
|  | Shri M. V. Rana (*Alternate*) |
| CSIR - National Metallurgical Laboratory, Jamshedpur |  | Dr Ashok K. Mohanty (*Alternate*) |
| Defence Metallurgical Research Laboratory, Ministry of Defence, Hyderabad |  | Shri S. S. Kalyan Kamal |
| Directorate General of Quality Assurance, Ministry of Defence, New Delhi |  | Shri Kesavamoorthy M |
|  | Shri E Suman. Kumar (*Alternate*) |
| Geological Survey of India, New Delhi |  | Shri Nitin Purushottam |
|  | Smt. Sanjukta Dey Pal (*Alternate*) |
| Hindalco Industries Limited, Mumbai |  | Shri Krishanu Mahapatra |
|  | Shri Ashutosh Acharya (*Alternate*) |
| Indian Metals and Ferro Alloys Limited, Bhubaneswar |  | Shri Dinesh Kumar Mohanty |
| JSW Steel Limited, Mumbai |  | Shri Kotrabasavaraju |
|  | Shri Marulasiddesha U. M. (*Alternate*) |
| Jawaharlal Nehru Aluminium Research Development and Design Centre, Nagpur |  |
|  | Dr Upendra Singh |
| National Aluminium Company Limited, Bhubaneswar |  | Smt Sukla Nandi |
|  | Shri Debananda Bhattacharyya (*Alternate*) |
| National Mineral Development Corporation, Hyderabad |  | Dr Saroj Kumar Sahu |
|  | Shri Ashish Shrivastava (*Alternate*) |
| National Test House, Kolkata |  | Dr Rajeev Kumar Upadhyay |
|  | Shri Akbar H. (*Alternate*) |
| Shriram Institute for Industrial Research, Delhi |  | Shri Dr Laxmi Rawat |
|  | Shri Puneet Kapoor (*Alternate*) |
| Research Designs and Standards Organization (RDSO), Lucknow |  | Shri Sandeep |
|  | Smt Sunia (*Alternate*) |
| Steel Authority of India Limited - Salem Steel Plant, Salem |  | Shri L. Sivakumar |
|  | Shri Vivekanandhan G. (*Alternate*) |
| TRL Krosaki Refractories Limited, Belpahar |  | Shri S. K. Subudhi |
| Tata Steel Limited, Kolkata |  | Shri Dr Jatin Mohapatra |
|  | Dr Ravikrishna Chatti (*Alternate*) |
| BIS Directorate General |  | Shri Sanjiv Maini, Scientist ‘F’/Senior Director and Head (Metallurgical Engineering) [Representing Director General (*Ex-officio*)] |

*Member Secretary*

Shri Ashish Prabhakar Wakle

Scientist ‘D’/Joint Director

(Metallurgical Engineering), BIS