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उपयोग करके कार्बन नैनोट्यूब नमूनों के गुणधर्म
(पहला पुनरीक्षण)

**Nanotechnologies —
Characterization of Carbon Nanotube
Samples Using Thermogravimetric
Analysis**
(First Revision)

ICS 07.120

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NATIONAL FOREWORD

This Indian Standard (First Revision) which is identical to ISO/TS 11308 : 2020 'Nanotechnologies — Characterization of carbon nanotube samples using thermogravimetric analysis' issued by the International Organization for Standardization (ISO) was adopted by the Bureau of Indian Standards on the recommendation of the Nanotechnologies Sectional Committee and approval of the Metallurgical Engineering Division Council.

This standard was first published in 2017 by adoption of ISO/TS 11308 : 2011. The first revision of this standard has been undertaken to align with the latest version ISO/TS 11308 : 2020 under dual numbering system to harmonize it with the latest developments that have taken place at international level.

The main change compared with the previous edition is as follows:

- a) A generalization has been made from single-walled carbon nanotubes to all forms of carbon nanotubes (including multi-wall).

The text of ISO standard has been approved as suitable for publication as in Indian Standard without deviations. Certain terminologies and conventions are, however, not identical with those used in Indian Standard. Attention is especially drawn to the following:

- a) Wherever the words 'International Standard' appear, referring to this standard, they should be read as 'Indian Standard'; and
- b) Comma (,) has been used as a decimal marker while in Indian Standards, the current practice is to use a point (.) as the decimal marker.

In this adopted standard, reference appears to certain International Standards for which Indian Standards also exist. The corresponding Indian Standards which are to be substituted in their place are listed below along with their degree of equivalence for the edition indicated:

<i>International Standard</i>	<i>Corresponding Indian Standard</i>	<i>Degree of Equivalence</i>
ISO/TS 80004-3 : 2020 Nanotechnologies — Vocabulary — Part 3: Carbon nano-objects	IS 17003 (Part 3) : 2022/ISO/TS 80004-3 : 2020 Nanotechnologies — Vocabulary: Part 3 Carbon nano- objects	Identical

For the purpose of deciding whether a particular requirement of this standard is complied with, the final value, observed or calculated, expressing the result of a test or analysis shall be rounded off in accordance with IS 2 : 2022 'Rules for rounding off numerical values (*second revision*)'. The number of significant places retained in the rounded off value should be the same as that of the specified value in this standard.

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Introduction

Carbon nanotubes (CNTs) are allotropic forms of carbon with cylindrical nanostructures. As a result of their geometric structures, these materials exhibit unique mechanical, thermal and electrical properties^{[1][2][3][4][5]}. CNTs are synthesized by several different methods, including pulsed laser vaporization, arc discharge, high pressure disproportionation of carbon monoxide and chemical vapour deposition (CVD)^{[6][7][8]}. These processes typically yield a heterogeneous mixture of CNTs and impurities, often requiring post-synthesis purification. Commonly observed impurities include other forms of carbon [e.g. fullerenes, amorphous carbon, graphitic carbon, single-wall carbon nanotubes (SWCNTs) and multi-wall carbon nanotubes (MWCNTs) outside the desired size or chirality range], as well as residual metallic catalyst nanoparticles. Purification can be accomplished using gaseous, chemical or thermal oxidation processes^{[9][10][11][12]}.

Thermogravimetric analysis (TGA) measures changes in the mass of a material as a function of temperature and time, which provides an indication of the reaction kinetics associated with structural decomposition, oxidation, pyrolysis, corrosion, moisture adsorption/desorption and gas evolution. By examining the reaction kinetics for a given sample, the relative fraction of different constituents present can be either quantitatively or qualitatively determined.

TGA is one of a number of analytical techniques that can be used to assess impurity levels in samples containing CNTs^{[14][15][16][17][18][19][20][21][22]}. For CNT-containing samples, TGA is typically used to quantify the level of non-volatile impurities present (e.g. metal catalyst particles). TGA is also used to assess thermal stability of a given sample, providing an indication of the type(s) of carbon materials present. Recent advances in TGA instrumentation enable better resolution during analysis. However, TGA alone is not specific enough to conclusively quantify the relative fractions of carbonaceous products within the material. Therefore, the information obtained from TGA should be used to supplement information gathered from other analytical techniques in order to achieve an overall assessment of the composition of a CNT sample^{[23][24][25][26][27][28][29]}.

Indian Standard

NANOTECHNOLOGIES — CHARACTERIZATION OF CARBON NANOTUBE SAMPLES USING THERMOGRAVIMETRIC ANALYSIS

(*First Revision*)

1 Scope

This document gives guidelines for the characterization of carbon nanotube (CNT)-containing samples by thermogravimetric analysis (TGA), performed in either an inert or oxidizing environment. Guidance is provided on the purity assessment of the CNT samples through a quantitative measure of the types of carbon species present as well as the non-carbon impurities (e.g. metal catalyst particles) within the material.

In addition, this technique provides a qualitative assessment of the thermal stability and homogeneity of the CNT-containing sample. Additional characterization techniques are required to confirm the presence of specific types of CNT and to verify the composition of the metallic impurities present.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO/TS 80004-3, *Nanotechnologies — Vocabulary — Part 3: Carbon nano-objects*

3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO/TS 80004-3 and the following apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <http://www.electropedia.org/>

3.1

primary oxidation temperature

$T_{ox'}$
temperature at which the most intense peak occurs in the first derivative thermogravimetric curve

3.2

thermal stability

dimensional stability of a solid material heated under specified conditions

Note 1 to entry: Thermal stability can be affected by the relative fraction of material *constituents* (3.4) in the sample as well as physical characteristics of the nanotube materials, such as diameter, length, defect state or surface treatment.

3.3

homogeneity

degree to which a property or a *constituent* (3.4) is uniformly distributed throughout a quantity of material

EXAMPLE Primary oxidation temperature.

3.4 constituent

component present in a carbon-nanotube-containing sample

Note 1 to entry: A carbon-nanotube-containing sample is often comprised of different carbon and non-carbon materials and is identified by oxidation peaks in the thermogravimetric analysis curve and by residual weight.

3.5 monotypic

material consisting of only one type of carbon nanomaterial

Note 1 to entry: When multi-walled carbon nanotubes are present, monotypic samples may contain a narrow range of diameters and lengths.

Note 2 to entry: A typical carbon nanotube sample comprises several types of carbon nanomaterials, including amorphous carbon, fullerenes, single-wall carbon nanotubes and multi-wall carbon nanotubes.

3.6 purity

measure of the fraction (percentage weight or mass fraction) of impurities within a given sample

Note 1 to entry: Thermogravimetric analysis alone cannot conclusively quantify the relative fractions of any and all carbonaceous products within the material. It can, however, quantify the level of non-volatile (e.g. metal catalyst) impurities, which is one measure of purity.

3.7 quality

overall assessment of the carbon nanotube sample

Note 1 to entry: A high quality carbon nanotube material is taken as a material with *high purity* (3.6), structural integrity and *homogeneity* (3.3).

Note 2 to entry: Thermogravimetric analysis can partly contribute to the quality assessment of carbon-nanotube-containing material by providing its residual weight and oxidation temperature.

Note 3 to entry: A carbon nanotube material may have a high purity level (i.e. a net mass fraction of 100 %) but it may have a considerable amount of damage, which can alter or destroy its physical properties, thereby deteriorating the quality of the material.

4 Symbols and abbreviated terms

CNT	carbon nanotube
CVD	chemical vapour deposition
DSC	differential scanning calorimetry
DTGC	derivative thermogravimetric curve (sometimes known as the “derivative weight loss curve”)
HiPco	high pressure CO conversion
MWCNT	multi-wall carbon nanotube
SWCNT	single-wall carbon nanotube
TGA	thermogravimetric analysis
T_{ox}	oxidation temperature
W_{res}	residual mass of the sample after heating

5 Principles of TGA

5.1 Measurement

At the basic functional level, TGA measures the change in mass of a material as a function of temperature as it is heated at a specified rate. In order to accomplish this, TGA requires the precise measurements of mass, temperature and temperature change. The change in mass of a material is related to the composition of the material and its thermal reactivity with the atmospheric conditions of the measurement. TGA analysis of CNT samples is most commonly performed in an oxidizing atmosphere, but can also be done with inert, reducing or other atmospheric conditions to probe different thermal reaction kinetics. Mass loss relative to an increase in temperature can result from the removal of absorbed moisture, solvent residues, chemically bound moieties and/or the thermal or oxidative decomposition of product.

TGA alone cannot identify the volatile materials released during heating; analytical techniques such as mass spectrometry (MS), gas chromatography (GC) and Fourier-transform infrared spectroscopy (FTIR) can be combined with TGA in order to identify volatile materials by coupling the appropriate instrumentation to the exhaust. Similarly, with respect to CNT-containing materials, TGA cannot by itself identify the different carbon forms present within the material. What it does do is determine the temperature at which the carbon species oxidize, which can be indicative of the identity of the species, as well as provide a quantitative measure of the non-volatile component.

When a CNT-containing sample is subjected to elevated temperatures in the presence of air, the carbon species present will oxidize into gaseous compounds such as CO or CO₂. The residue comprises non-volatile materials, which for the most part are metal impurities.

5.2 Exothermic and endothermic reactions

Some CNT-containing samples have been observed to undergo combustive reactions during TGA analysis, resulting in rapid burning of material, possibly catalysed by residual metals in the sample. Such events are distinguished by a difference in temperature between the sample and the reference, but also a rapid change in sample mass with little or no change in reference temperature^[30].

6 Sampling

6.1 Sample pan selection

Sample pan size and type will vary depending on the instrument being used and the temperature range of interest. There is no restriction on the sample pan size so long as it is compatible with the instrument and it is capable of accommodating the required amount of CNT sample with minimal compaction (see [6.3](#) and the references within for a discussion of sample compaction). Aluminium, ceramic or platinum pans may be used depending on the experimental temperature range. Aluminium pans are the least likely to catalytically oxidize the CNT material, but they do not cover as wide of a temperature range. Ceramic and platinum pans are more likely to have adsorbed contaminants that can lead to inconsistent or even erroneous data. [Table 1](#) provides guidance to some of the available pans. Standard manufacturer recommended procedures should be followed to remove any residual material from previous samples prior to conditioning. To remove adsorbed moisture, it is recommended that the pans be conditioned by heating to at least 300 °C in an air environment prior to introduction of the CNT sample. If the pans are not used immediately after conditioning, they should be stored in a dry box or desiccator until loading to prevent the reintroduction of moisture.

Table 1 — Sample pan selection guidance for TGA of CNTs

Pan material	Temperature range	Comments
Aluminium	Ambient to 600 °C	Aluminium pans are considered disposable by manufacturers, which is beneficial in eliminating contamination. However, the low maximum temperature means they can only be used when it is certain that all the CNT material will burn off before 600 °C.
Ceramic	Ambient to 1 200 °C and above	Porous ceramic will easily pick up moisture from the atmosphere, so it is especially important to condition the pans for consistent results. Ceramic pans are capable of use above 1 200 °C; however, most TGA instruments are limited to an upper temperature of 1 200 °C.
Platinum	Ambient to 1 000 °C	It is important that the platinum pan is rated for high temperature use otherwise the maximum temperature is only 750 °C.

6.2 Sample size

The controlling factor in the selection of sample size is the bulk density of the CNT material. As-produced samples can be more difficult to accommodate in TGA pans because of their lower bulk density, whereas purified materials are condensed during the purification processes. If the minimum recommended amount of the sample is too fluffy for the available TGA pan, slight compacting with a spatula may be used to contain the sample within the pan.

Additional details on sampling can be found in Reference [31].

For dry powder samples:

- a) use a minimum of 1 mg of sample or the amount recommended for the instrument by the manufacturer for the specific pan size being used, whichever is greater;
- b) load samples into pan and store in a dry environment for at least 48 h prior to measurement; if possible, load samples in a controlled environment such as a glove box or nano-hood to prevent the airborne release of nanotubes;
- c) weigh samples at an ambient temperature on a microbalance.

6.3 Sample compaction

Compaction of a powder using a press is a common method of preparation for TGA and DSC measurements of powder samples. The effects of high pressure compaction of SWCNT samples have been investigated^[31] and it has been found that compaction in a KBr pellet die (such as those commonly used for the preparation of samples for infrared spectroscopy) can influence the observed oxidation temperatures, though no effect was found on the residual mass values. Details of necessary provisions concerning compaction are described further in B.3.

The following rules regarding sample compaction apply:

- a) do not use high pressure sample compaction (e.g. with a pellet die);
- b) slight compaction by low pressure pressing with a spatula is acceptable to contain the full sample within the pan.

7 Test method

The following procedure outlines the minimum requirements for obtaining TGA data that will allow for a reliable characterization of CNT samples. At a minimum, this procedure should be repeated three times for each sample. A typical run usually takes approximately 2 h, depending on the ramp rates used.

- a) Calibrate the TGA instrument according to the manufacturer's protocols to ensure the proper temperature and weight measurement.
- b) Prepare the TGA instrument by first taring an empty sample pan in the TGA balance. On a microbalance, weigh and record a minimum of 1 mg of sample and transfer into the pan. If possible, perform all weighing and transfer operations in a dry environment. The samples should be kept in a desiccator for 48 h to remove any retained moisture. If the equipment allows it, store the loaded pan in the same way. Alternatively, if the tare function is not available in the instrument (as may be the case with older instrumentation), weighing the sample in a dry environment is acceptable.
- c) Transfer the sample, or the loaded pan, to the TGA instrument for analysis.
- d) Set the maximum temperature for the scan based on the anticipated composition of the sample and the sample pan being used. If the sample is unknown, set the maximum temperature to 900 °C or the highest temperature that can be used with the sample pan selected.
- e) Set the temperature ramp rate to a constant rate between 1 °C/min and 10 °C/min for the entire temperature range. Slower heating rates allow more time for reactions to occur.

NOTE 1 If there are known or suspected organic impurities in the sample, the sample can first be heated to 120 °C with an inert gas flow and held at this temperature for 30 min prior to heating over the entire temperature range. This additional heating step can also be used if the sample is unknown to ensure that there is sufficient time for evolution of any organic impurities.

- f) Set the gas flow rate based on the manufacturer's recommendation for the particular TGA instrument. If no recommendation is given, set the flow rate to no less than 100 ml/min.

NOTE 2 The flow rate needed for successful operation will be dependent on the instrument geometry. If no flow rate is recommended by the manufacturer, the most important consideration is that the flow rate provides an optimal burn rate of the sample while minimizing any buoyancy effects on the sample weight determination.

NOTE 3 Air or oxygen is used as the gas for oxidative decomposition studies while an inert gas such as nitrogen or argon is used for pyrolytic decomposition studies. Other gases can be used for different situations.

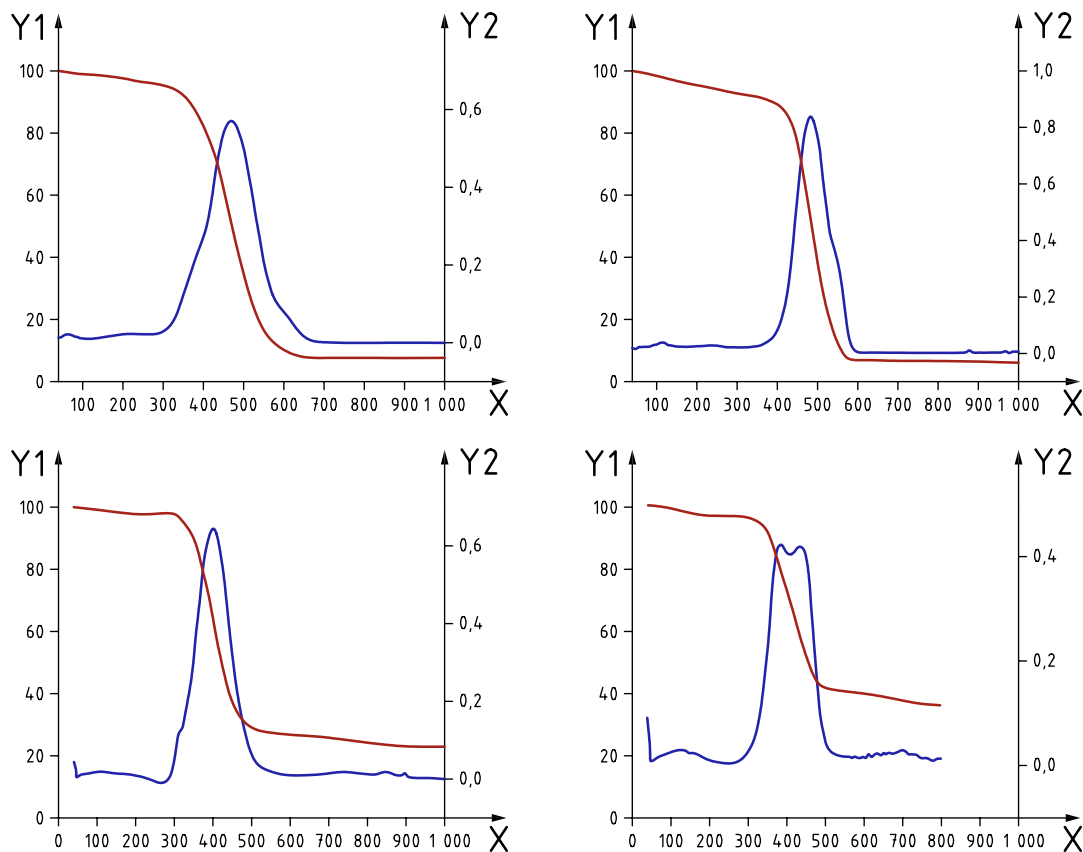
NOTE 4 Cooling rate is instrument dependent.

- g) After completion of the measurement, record the residual mass (W_{res}) value for each scan at room temperature on a microbalance.
- h) Record the oxidation temperature (T_{ox}) for each peak within a scan. The overall T_{ox} for each species attributing to the TGA curve is determined from the mean value of the three runs. T_{ox} for the particular species is then documented as the mean value plus and minus the standard deviation.

8 Data interpretation and results

8.1 General

The following are guidelines for the interpretation of the TGA curves and the type of information used to evaluate CNT-containing materials. An example of TGA curves for four different CNT samples (each produced by a different method) is shown in [Figure 1](#).



Key
X temperature (in °C)
Y1 weight (in %)
Y2 deriv. weight (in %/°C)

Figure 1 — TGA curves for CNT samples produced by different methods^[32]

8.2 Non-carbon content

The non-carbon content of the CNT-containing sample is assessed through the W_{res} value. This value is acquired from both the TGA data and a microbalance value. From the TG curve, W_{res} is recorded as the mass remaining above 800 °C. This value is compared to the microbalance weight in order to assess if there is a systematic error due to buoyancy effects caused by the air flow in the instrument. W_{res} can be expressed as either the actual weight that remains or as a percentage of the original weight of the sample. To report the non-carbon content of a CNT-containing sample, W_{res} will be expressed as the mean percentage weight together with the standard deviation from at least three TGA measurements.

NOTE The determination of non-carbon content in the original CNT sample from W_{res} can be inaccurate as some contributors to the residual will change oxidation state during heating, resulting in either a decrease or increase in weight. W_{res} will, however, still provide a good approximation to the overall non-carbon impurity component of the CNT material, especially when comparing samples from the same production method (see [A.2](#)) that will likely have the same impurities.

It is recommended that the user verify the oxidative stability of the metals used as catalysts by conducting TGA analysis of the catalyst at identical heating and air flow rates. These measurements will establish whether W_{res} measures metals, metal oxides or a mixture of the two. If the catalyst composition is unknown, the largest temperature range should be used.

8.3 Constituents

Most production methods for CNTs are not 100 % efficient in the conversion of the source carbon to a single species. Single-wall production methods do not eliminate multi-wall tubes and vice versa. Additional forms of carbon such as fullerenes or amorphous carbon also cannot be fully eliminated at the time of production. The presence of multiple constituents can be qualitatively determined from TGA data by determining the number of oxidation peaks present in the DTG curve^[34]. While it is difficult to assign any particular carbon form to a specific oxidation peak, especially as the number of constituents in the sample increases, it is commonly agreed upon that multiple peaks arise due to the presence of different carbon types (see [A.3](#)).

NOTE TGA data from relatively pristine samples have shown that single, double and multi-wall CNTs have unique ranges of oxidation temperatures, which can be used to distinguish between the different CNT constituents if it is known that there is minimal overlap with any non-CNT carbon constituents^[34].

8.4 Thermal stability

The thermal stability of a sample of CNT material is the dimensional stability of a solid material heated under specified conditions. Thermal stability of a sample of CNT material can be affected by the relative fraction of material constituents in the sample as well as physical characteristics of the nanotube materials, such as diameter, length, defect state or surface treatment. The parameter used to assess thermal stability is the primary oxidation temperature, which is the temperature at which the highest fraction of carbon content oxidizes (see [A.4](#) and Reference [\[30\]](#)).

8.5 Homogeneity

The homogeneity of CNT materials is established in TGA by the constituency, thermal stability and scatter in the T_{ox} and W_{res} values of multiple runs (see [A.5](#) and Reference [\[30\]](#)). A material is considered sufficiently homogeneous if it meets pre-defined quantitative limits for the following criteria.

The TGA data from a minimum of three runs:

- should produce the same set of oxidation peaks (same constituency);
- should have a similar primary T_{ox} (thermal stability) from run to run;
- should have T_{ox} and W_{res} values with a narrow standard deviation (see [Annex A](#)).

If all three conditions are not met, the material cannot be considered homogeneous.

8.6 Purity

The purity of either a SWCNT or a MWCNT sample is established by the mass fraction of the desired CNTs relative to both the carbon and non-carbon impurities within the material. TGA alone can only reliably provide purity assessment relative to the non-carbon impurities through the W_{res} value. A material with lower residual values is therefore considered a material with better purity relative to the non-carbon impurity content. To clearly define the overall purity of a material, TGA results must be coupled with information from other techniques (see [A.6](#)).

8.7 Quality

As with purity assessment, the quality assessment of a CNT sample cannot be completely determined by TGA. However, two of the material characteristics (purity and homogeneity) required to establish the quality of a material can be identified by TGA, and are particularly useful when describing CNT materials^[30].

A CNT sample that produces TGA data showing a low W_{res} value and high homogeneity (reproducible TGA data from run to run) can be considered to have uniform quality relative to TGA. The actual quality of the CNT sample can only be established by coupling information from other analytical techniques

such as elemental analysis for the composition or Raman spectroscopy for the level of defects in the material.

9 Uncertainties

Uncertainty can occur in the exact measurement of the non-carbon content present within a CNT sample. The non-carbon elements typically found in as-produced materials might react at elevated temperatures to form non-volatile oxides or carbides. In this case, the measure of W_{res} will be higher than the actual weight of the non-carbon content.

On the other hand, some non-carbon elements might react to form volatile oxides, in which case the measured W_{res} may be lower than the actual non-carbon content. As recommended in 8.3, the response of the catalyst to heating can be determined by running it under the same conditions used for the samples. The W_{res} value can then be used to calculate the amount of catalyst in the material.

Finally, in TGA runs on highly pure nanotubes [minimal (less than 10 %) content of ash remaining after the completion of the TGA run], the W_{res} is sometimes negative, mainly because of drift of the TGA balance. This can happen even with regular calibration of the instrument. The long-term stability of the instrument (during a run of more than 3 h) is generally within 20 µg to 40 µg, which is equivalent to 2 % to 4 % of a 1 mg sample. The stability of the instrument can be quantified by running an empty sample pan under the same conditions used for the samples. Alternatively, the larger the amount of sample that can be used, the more negligible the 20 µg to 40 µg drift becomes.

Determination of the measurement uncertainty value may be done by following ISO/IEC Guide 98-3:2008.

10 Test report

In addition to the information required for reporting test results from ISO/IEC 17025, the following data should be included in the test report:

- a) sample information:
 - 1) lot number;
 - 2) manufacturer and production method used to synthesize CNT sample, if known (e.g. CVD from manufacturer A);
 - 3) weight of sample used:
 - i) weight from microbalance (run1: weight1, run2: weight2, run3: weight3, etc.);
 - ii) weight from TGA balance (run1: weight1, run2: weight2, run3: weight3, etc.);
- b) TGA curve analysis that is to be recorded for evaluation of material (report the actual curves as well):
 - 1) number of peaks in individual DTG curves (run1: 3 peaks, run2: 1 peak, run3: 2 peaks);
 - 2) primary oxidation temperature from individual DTG curves (run1: x °C, run2: y °C, run3: z °C);
 - 3) weight of the remaining ash from individual runs from the microbalance (run1: x mg, run2: y mg, run3: z mg);
 - 4) weight of the remaining ash from individual runs from the TGA balance (run1: x mg, run2: y mg, run3: z mg);
 - 5) residual weight from individual TGA curves (run1: x%, run2: y%, run3: z%);
 - 6) calculation of the average residual weight with standard deviation (x% ± y%);
 - 7) heating ramp;

- 8) temperature range;
 - 9) flow rate and type of gas used;
- c) TGA data interpretation and results:
- 1) constituency: monotypic or multiple constituents;
 - 2) thermal stability: when definable, list the average T_{ox} , with standard deviation, otherwise list as undefinable;
 - 3) homogeneity: state when the material can be considered sufficiently homogeneous if it meets pre-defined homogeneity criteria, otherwise state that it cannot be considered homogeneous;
- d) additional information:
- 1) brand and model of the TGA equipment used.

Annex A (informative)

Case studies

A.1 General

This annex gives examples on the use of W_{res} and T_{ox} values for the assessment of constituency, homogeneity, non-carbon content, purity, quality and thermal stability. TGA data were obtained on various CNT materials produced by arc discharge, CVD, high pressure disproportionation of carbon monoxide and pulsed laser vaporization.

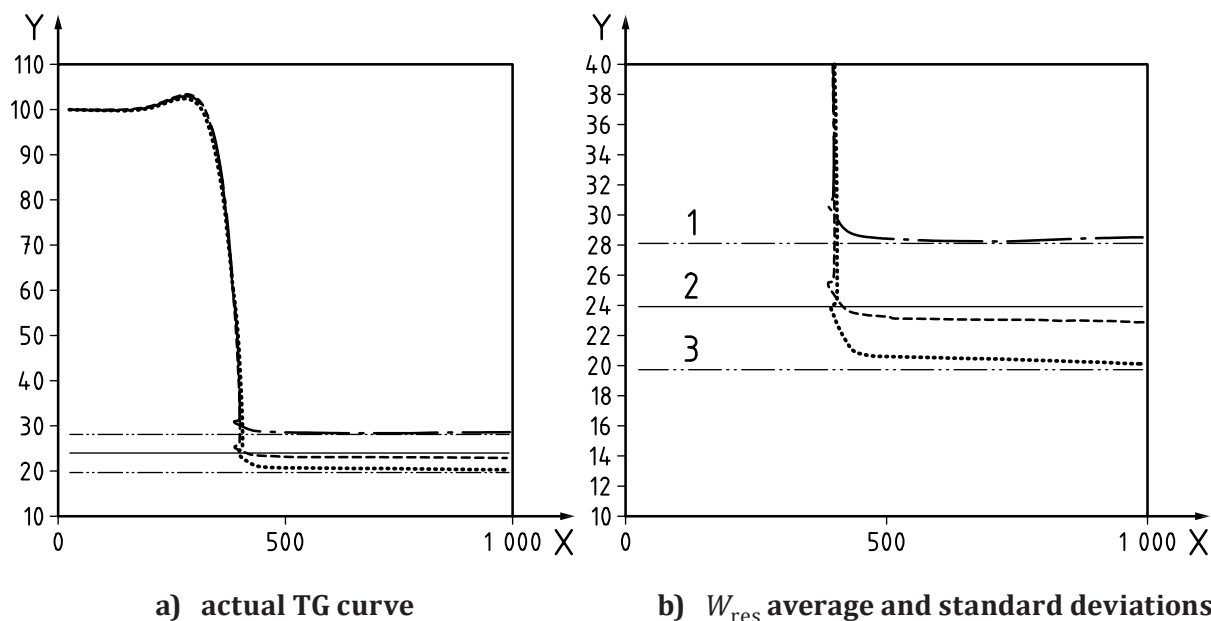
A.2 Evaluation of non-carbon content

A.2.1 Determination of non-carbon content

The non-carbon content is determined from weight measurements obtained from both the TGA apparatus and a microbalance before and after the run. The reason for this is to identify any possible sources of measurement error. Discrepancies may arise from buoyancy effects, thermal expansion of balance arms, loss of sample during transfer or moisture adsorption of the sample. Furthermore, the long-term stability of the instrument zero (during a run of more than 3 h) is generally within 20 μg to 40 μg , which is equivalent to 2 % to 4 % of a 1 mg sample. Weighing independently allows for greater confidence in the data.

The most representative measure of the W_{res} of a sample is taken as the lowest point in the TG curve. The mean value of the W_{res} and the standard deviation from multiple runs are to be calculated and used to report the non-carbon content (see [Figures A.1](#) and [A.2](#)). Similar calculations for the W_{res} as determined by the microbalance measurements are to be compared (see [Tables A.1](#) and [A.2](#)). Large differences between the two determinations would merit additional runs or re-calibration of the system.

Two factors which may influence the W_{res} determination are adsorbed water content and oxygen uptake from the non-carbon components. The water content can be easily accounted for by measuring the mass difference between the starting weight and the weight at which the TG curve first levels off, typically around 150 °C. Oxygen uptake due to the oxidation of non-carbon impurities is addressed in more detail in [A.2.2](#).



Key

— — — —	run 1	X	temperature (in °C)
.....	run 2	Y	percentage weight (in %)
— — — —	run 3	1	std. dev. = +4,2
— — — —	std. dev	2	average =
— — — —	average	3	std. dev. = -4,2

NOTE W_{res} average and standard deviations are calculated in [Table A.1](#)

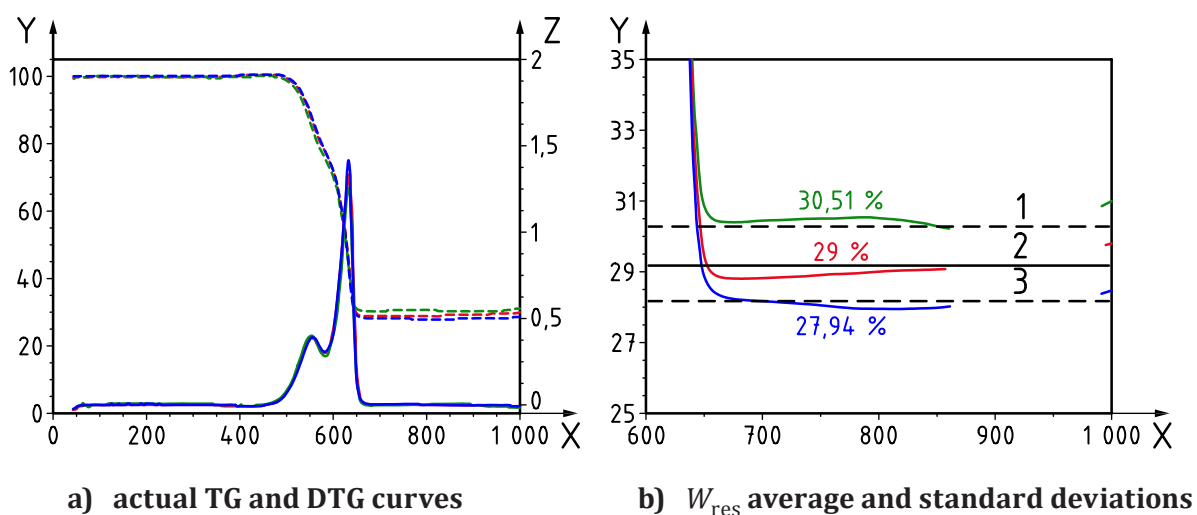
Figure A.1 — TGA results for a CNT sample

Table A.1 — Calculations of W_{res} average and standard deviations from three HiPco SWCNT runs

Parameter	Run 1	Run 2	Run 3	Average	Standard deviation
Sample weight: microbalance (in mg)	3,09	3,20	3,00	—	—
Sample weight: TGA (in mg)	3,22	2,98	2,84	—	—
Residual weight: microbalance (in mg)	0,63	0,65	0,65	0,64	0,01
Residual weight: TGA at 1 000 °C (in mg)	0,91	0,60	0,65	0,72	0,17
Residual weight: TGA at room temperature (in mg)	0,90	0,59	0,61	0,70	0,17
Amount of oxygen uptake (in mg)	0,09	0,07	0,10	—	—
Amount of H ₂ O desorption (in mg)	—	—	—	—	—
% residual weight: microbalance (uncorrected)	20,36	20,32	21,73	20,80	0,80

Table A.1 (continued)

Parameter	Run 1	Run 2	Run 3	Average	Standard deviation
% residual weight: TGA at 1 000 °C (uncorrected)	28,22	20,22	23,01	23,82	4,06



Key

- Run 1
- Run 2
- Run 3
- X temperature (°C)
- Y percentage weight (%)
- Z derivative percentage weight (%/°C)

NOTE W_{res} average and standard deviations are calculated in Table A.2.

Figure A.2 — Weight loss and derivative curves for as-produced CVD material

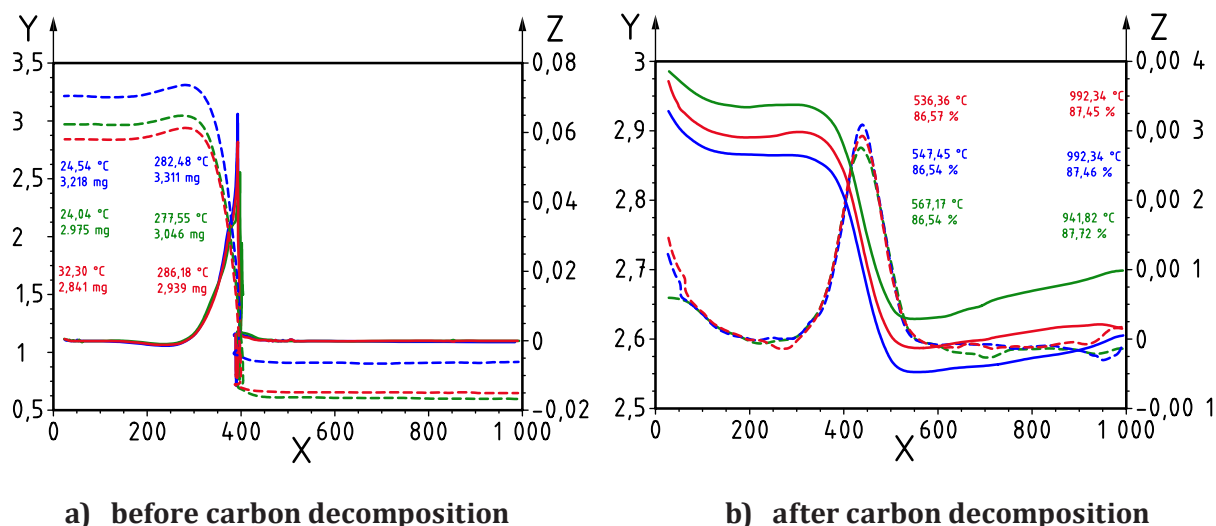
Table A.2 — Calculations of W_{res} and T_{ox} average and standard deviations from three repeat runs

Parameter	Run 1	Run 2	Run 3	Average	Standard deviation
Sample weight: microbalance (in mg)	1,37	1,23	1,37	—	—
Sample weight: TGA (in mg)	1,35	1,22	1,41	—	—
Residual weight: microbalance (in mg)	0,43	0,41	0,40	—	—
Residual weight: TGA at 800 °C (in mg)	0,39	0,37	0,39	—	—
% residual weight: microbalance (uncorrected)	31,39	33,33	29,20	31,31	1,69
% residual weight: TGA at 800 °C (uncorrected)	29,00	30,51	27,94	29,15	1,05
Primary T_{ox} (in °C)	632,55	631,73	633,43	632,57	0,69
Additional peak T_{ox} (in °C)	556,39	554,81	555,34	555,51	0,66

A.2.2 Oxidation of non-carbon content

The non-carbon content consists primarily of metal catalyst used in CNT synthesis, which can itself become oxidized under the TGA run conditions and influence the non-carbon content determination. Oxidation of the non-carbon is observed as weight increase in the TG curve and may occur before or after the oxidation of carbon species (see Figure A.3). In either case, it is difficult to quantify the extent of oxidation to the non-carbon components since TGA cannot identify the type of oxides formed.

However, the amount of oxygen uptake is to be recorded in order to provide a measure of uncertainty in the W_{res} determination. Furthermore, some oxides that form during a TGA run can be volatile, which adds additional complication into the W_{res} determination. This is difficult to measure in a stand-alone TGA. Without knowledge of this type of oxide formation, the W_{res} is taken as representative of the non-carbon content. Whether oxidation of the non-carbon content results in a volatile or non-volatile oxide, the variation in reactivity introduces uncertainty in the determination of the true non-carbon content.



Key

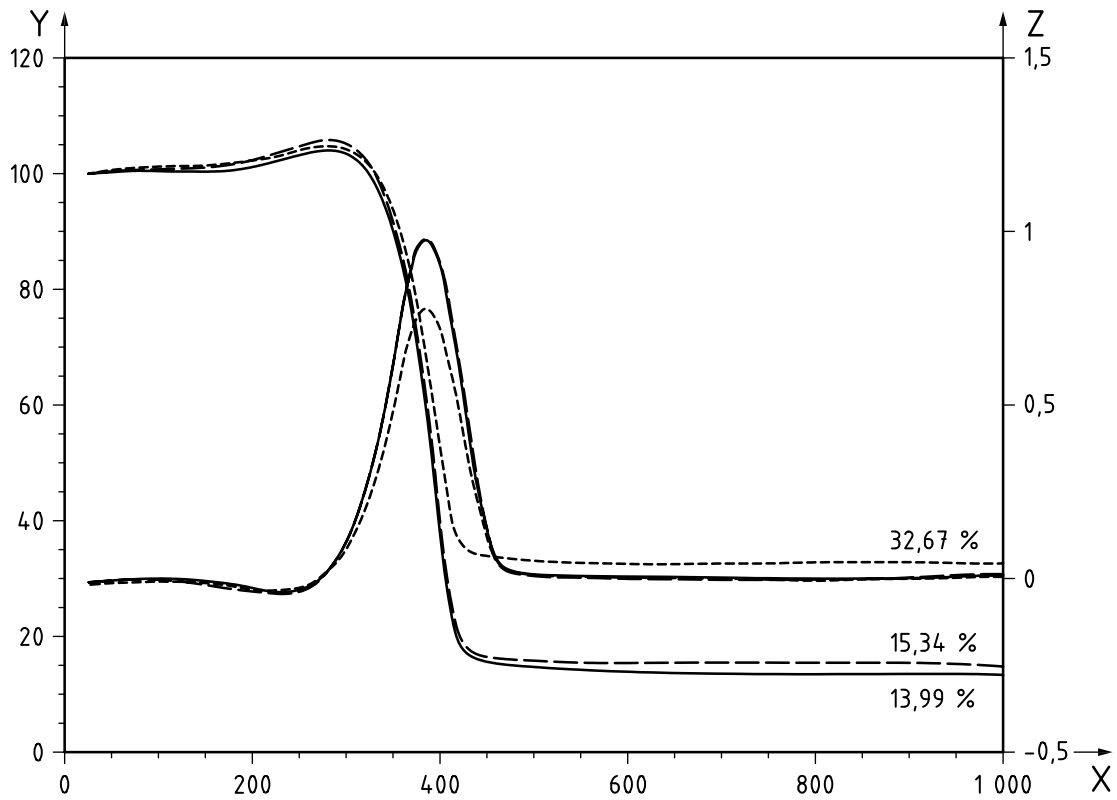
- X temperature (in °C)
- Y percentage weight (in %)
- Z derivative weight (in mg/°C)

Figure A.3 — Oxidation of non-carbon content before and after carbon decomposition

A.3 Constituency

The constituency of a CNT material is described as arising from the different carbon forms present within the material, as is observed in TGA by multiple peaks in the DTG curve (see [Figures A.2](#) and [A.5](#)). The presence of multiple peaks in the DTG curve represents a material with higher constituency. While it is difficult to assign any individual peak to a particular form of carbon, it is agreed upon that multiple peaks arise from different carbon species. These multiple peaks in the DTG curve may be attributed to isolated amorphous carbon^{[3][4][5]}, amorphous coated CNTs^[4], defective tubes, chemically derivatized tubes^[6], tubes of varying diameters or crystallinity^{[4][6]}, graphitic carbon, and the dispersion of the residual metal catalyst after purification.

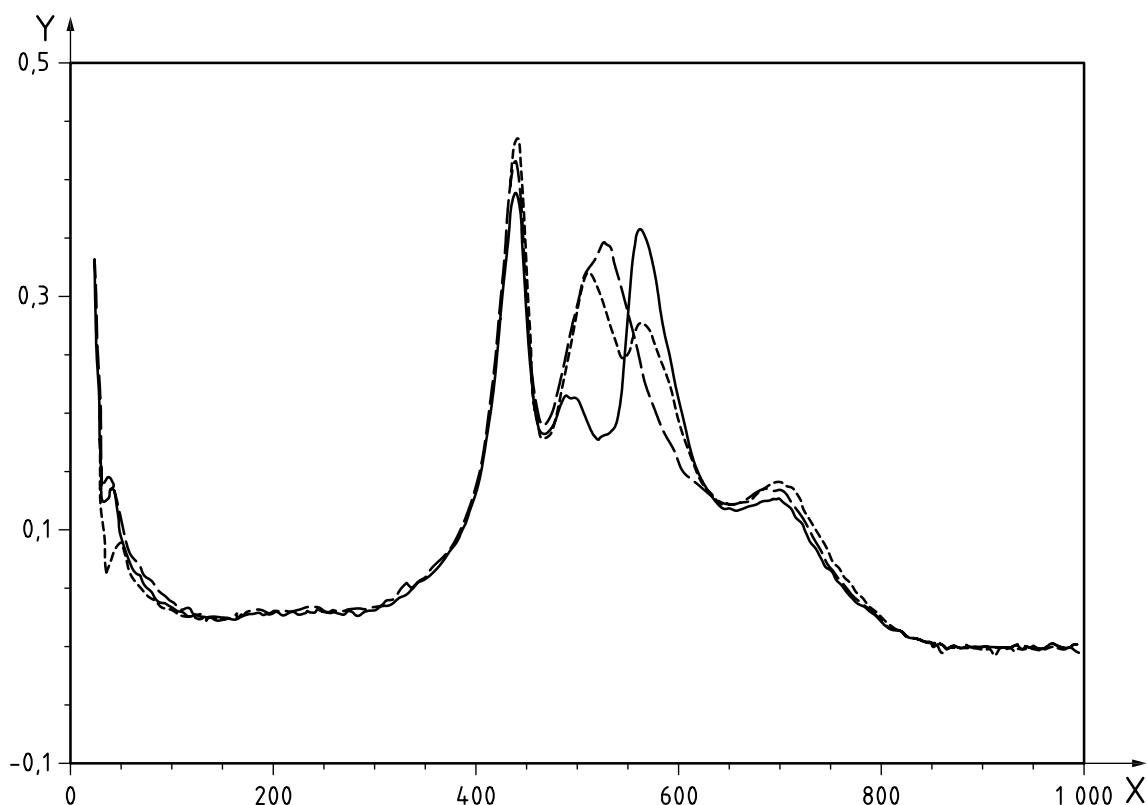
Uncertainty in the constituency can arise in CNT materials that exhibit combustible behaviour, which are marked in TGA by an abrupt drop-off in the DTG curve as well as a backwards trace in the TG curve [see [Figure A.3 a](#)]. This behaviour is more often observed in unpurified CNT materials that have fluffy morphology and greater metal content, and it is more probable with increased heating rate. This behaviour is explained by a rapid burning of the sample, resulting in a very quick release of a considerable amount of heat, causing a sharp increase in temperature followed by heat dissipation and a subsequent temperature drop. Combustion can complicate the constituency assessment since components with higher oxidation temperatures might be burned or blown out of the sample pan during the combustion.



Key

- X temperature (in °C)
- Y percentage weight (in %)
- Z derivative weight (in mg/°C)

Figure A.4 — Material with well-defined constituency and thermal stability but large deviation in the residual weight value resulting in low homogeneity



Key

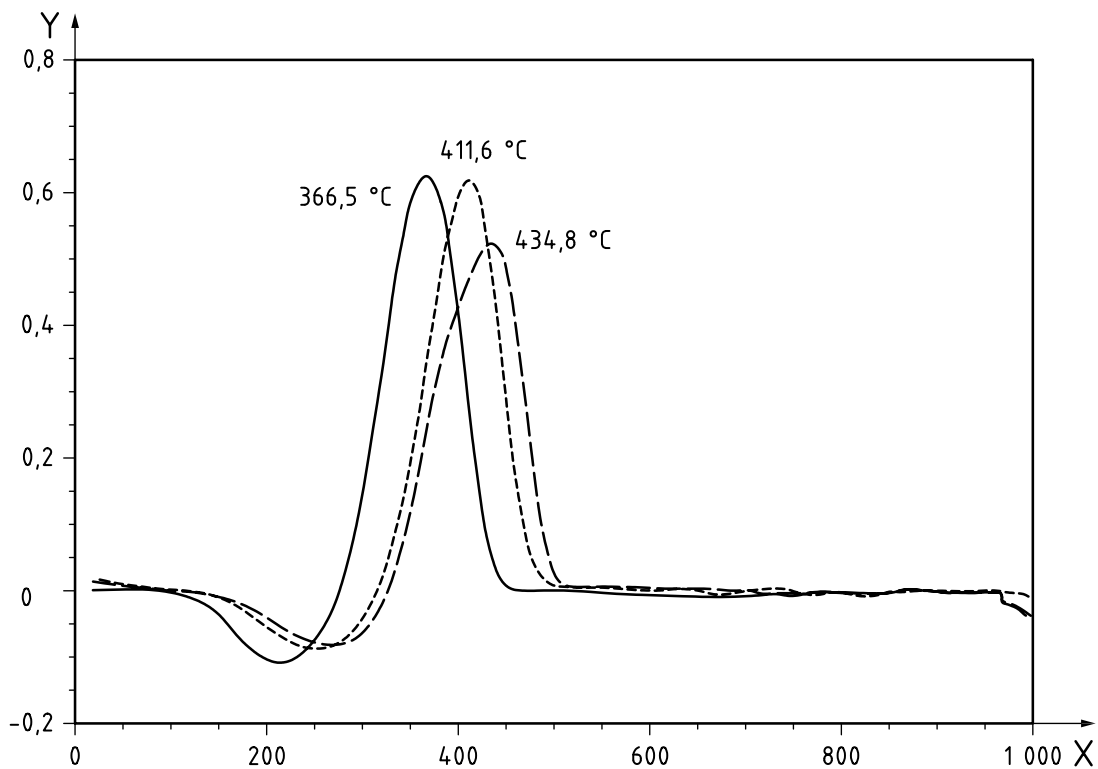
X temperature (in °C)

Y derivative weight (in mg/°C)

Figure A.5 — Material with low homogeneity as a result of variable constituency

A.4 Thermal stability

Thermal stability is a straightforward assessment as it is simply the most intense DTG peak for each run, which signifies the most abundant carbon species present in the sample. The intensity of the peak is used instead of the area under the peak (determining areas is not straightforward since this requires deconvolution of the DTG curve into multiple peaks). In addition, the background subtraction and curve shape may be cumbersome. On the other hand, the peak intensity is easy to identify and is indicative of a greater rate of mass loss. The thermal stability is also reported as the mean value of T_{ox} from the multiple TGA runs along with its standard deviation. If T_{ox} has large scatter in value (see [Figure A.6](#)) or is inconsistent in assignment (see [Figure A.7](#)), then the thermal stability cannot be defined.

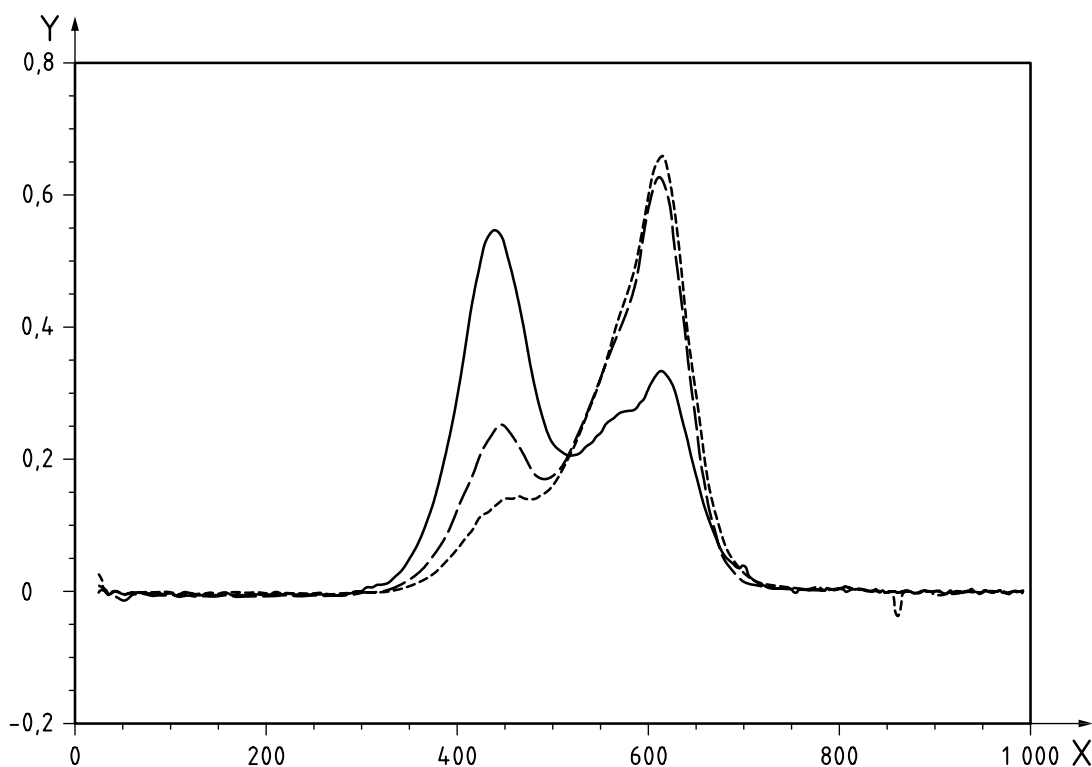


Key

X temperature (in °C)

Y derivative weight (in mg/°C)

Figure A.6 — Material with essentially one constituent but large scatter in primary oxidation temperature resulting in an undefined primary oxidation and low homogeneity



Key

X temperature (in °C)

Y derivative weight (in mg/°C)

Figure A.7 — Material with variable constituency and thermal stability

A.5 Homogeneity

A.5.1 General

In this subclause, several examples are presented to help explain the assessment of homogeneity through variations in the non-carbon content, constituency and thermal stability. The determination of homogeneity is influenced by several parameters, which will be described individually. Examples of TGA features not consistent with a homogeneous material are shown in [Figures A.4 to A.7](#).

A.5.2 Variation in non-carbon content

The homogeneity of a batch of CNT material is in part established by the uniform distribution of non-carbon content throughout the batch. If there is not a uniform distribution of the non-carbon component in the material, there will be large scatter of the W_{res} values from multiple runs. This in turn will result in W_{res} values with a standard deviation greater than 2,0 %, the acceptable limit (see [Figure A.4](#)). In this case, the material will not be considered homogeneous. On the other hand, if the standard deviation of the W_{res} values is less than or equal to 2,0 %, the material may be considered homogeneous with respect to the quantity of the non-carbon content.

A.5.3 Variation in the constituency

Constituency is another parameter that helps define the homogeneity as assessed through TGA. Uniform constituency from run to run is a trait of a homogeneous material. If the concentration of different carbon components varies among the samples in the same batch, the relative intensities of the oxidation peaks in the DTG curves will also vary from run to run. Because morphology and catalyst content can influence the burn rates of carbon material, it is difficult to quantify the constituency;

however, the qualitative analysis can still be used to assess the homogeneity. If from run to run there are variations in the number or relative intensities of the oxidation peaks present (see [Figure A.5](#)) or if the primary oxidation temperature shifts (see [Figure A.7](#)) by more than an acceptable amount, then the material cannot be labelled as homogeneous as defined by TGA.

Combustion can complicate the assessment of homogeneity since sample material can be blown out of the pan when this occurs. If combustion occurs in one run but not the other two, the homogeneity cannot be defined. However, if all three runs display a combustive behaviour, the material is considered homogeneous as the morphology is the same throughout the batch.

A.5.4 Variation in the thermal stability

Another factor used for the assessment of homogeneity is the variation in the thermal stability of multiple TGA runs. This variation is established by the value of the standard deviation of the primary T_{ox} . If the standard deviation in T_{ox} is greater than the value of the heating rate (i.e. if the standard deviation exceeds 5 °C), the material may not be considered homogeneous (see [Figure A.6](#)).

NOTE The heating rate directly influences the kinetics of oxidation (see [B.2](#)). Therefore, the heating rate is chosen as the basis to discount any lag in the oxidation process due to variation in the activation energy, thermal conduction through the material in proper air flow or inaccuracy in the thermocouple measurements.

A.6 Purity assessment

TGA by itself is unable to provide a measure of the overall purity of CNT material since it is limited in the information relative to the types of impurities which can be found in CNT material. TGA can only provide one piece of the puzzle regarding impurity levels with the material: the amount of non-carbon content through the W_{res} value. Even if the oxidation temperatures of pure SWCNTs were known and accepted, for example, there are other carbon types that have a similar enough oxidation temperature to make them indistinguishable by TGA. A true purity assessment can be accomplished when TGA is coupled to other analytical techniques since TGA can provide the information on the non-carbon impurity levels with the material.

A.7 Quality assessment

The quality of a CNT material cannot be clearly defined through the use of TGA. TGA can, however, indicate the likelihood for a material to have good quality. The quality of the CNT material is taken as a material with high purity, structural integrity and homogeneity. The high purity of the CNT material can be assessed partly by obtaining a low value of W_{res} in the TGA runs. Another way that TGA can contribute to the quality assessment of the material is to compare the structural integrity between runs. While a CNT material could have a high degree of purity, it could have enough damage to its chemical structure that its physical properties can be altered. Defects^[7], such as Stone-Wales defects^{[8][9][10]}, or severe oxidative damage in the form of vacancies or sp^3 hybridization, can destroy the structural integrity. The structural integrity can be evaluated by the primary T_{ox} in the TGA. A good-quality CNT material should possess a low level of variation in the W_{res} , constituency and T_{ox} values.

Annex B (informative)

Effects of operating parameters on TGA analysis

B.1 General

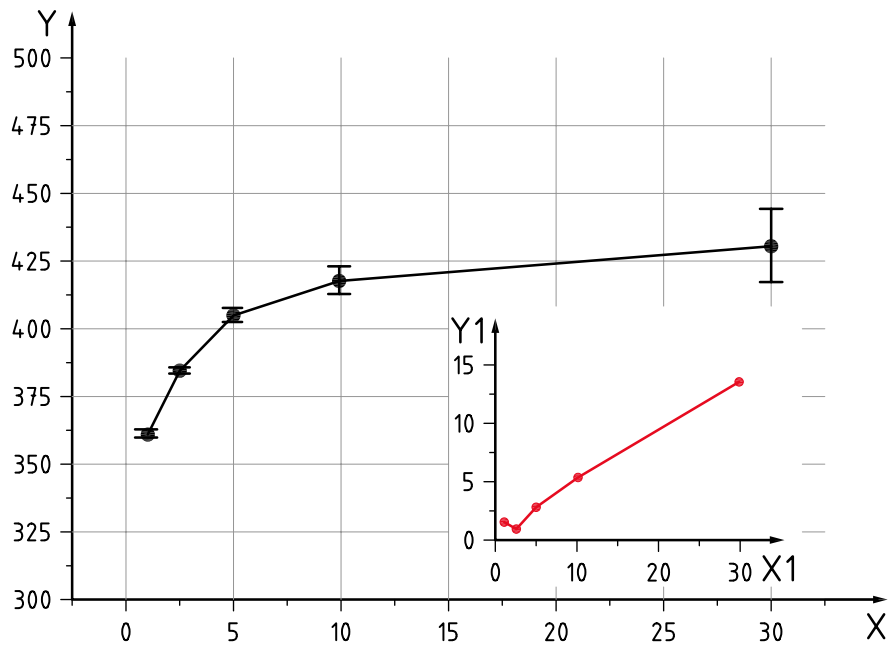
In this annex, the influence of operating parameters on TGA results is briefly explained, the effects of heating rate and sample compaction are presented, and a technical explanation of combustion is provided. For more in-depth information, refer to the relevant part of Reference [35].

B.2 Influence of heating rate

TGA experiments were done with the following heating rates: 1 °C/min, 2,5 °C/min, 5 °C/min, 10 °C/min, 30 °C/min, and 100 °C /min. [Figure B.1](#) shows that the mean value of T_{ox} increases gradually from 360 °C to 430 °C as the heating rate increases from 1 °C/min to 30 °C/min. The origin of such a significant change in T_{ox} (70 °C) is attributed to the kinetics of the oxidation reaction. Experimentally the change may be influenced by the limited rate of heat conduction into the sample under the high heating rate such as 100 °C/min. It is difficult to reliably determine T_{ox} (and its standard deviation) for the experiment with a 100 °C/min heating rate due to the very broad transition with several peaks that are not reproducible.

The value of W_{res} and its standard deviation are also dependent on the heating rate. [Figure B.2](#) shows that W_{res} for 1 °C/min, 2,5 °C/min and 5 °C/min heating rates are well within one standard deviation (which is nearly constant), while above 5 °C/min W_{res} becomes smaller and its standard deviation sharply increases. This observation can be explained by spontaneous combustion of the SWCNT materials above the heating rate of 5 °C/min (i.e. the heat released in the exothermic reaction is enough to sustain rapid burning of the sample). Therefore, it is important to collect TGA data with heating rates that do not allow combustion.

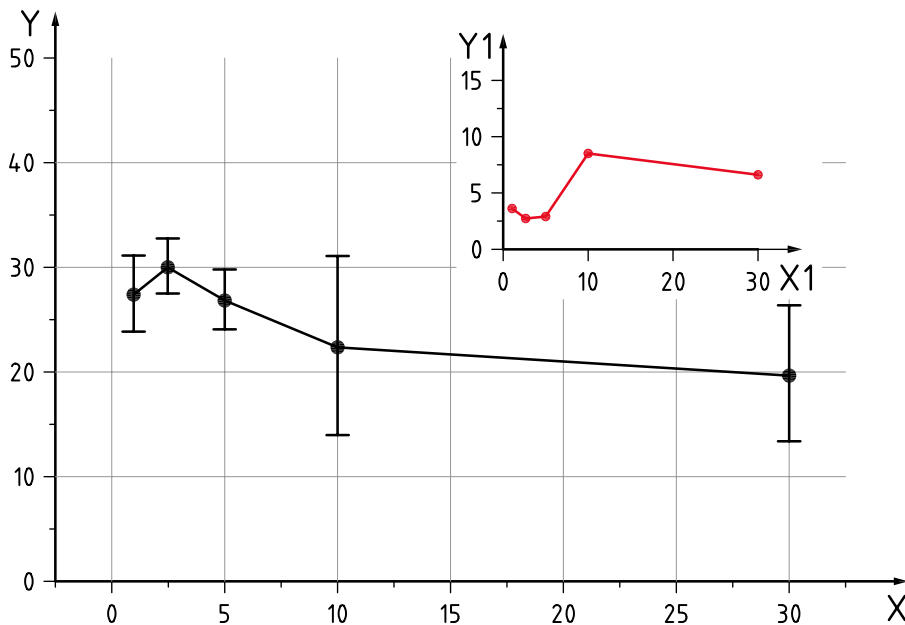
Selection of the heating rate is also of practical importance. Usually a sample has to be heated to at least 1 000 °C, which requires 13,3 h at a rate of 1 °C/min, compared to 8 min at 100 °C/min. Heating quickly saves time, so the majority of researchers have used 10 °C/min to 20 °C/min rates. Based on the discussion above, 5 °C/min has been selected as a compromise, as each run takes less than 3 h and combustion is avoided for most types of samples.



Key

- | | | | |
|---|------------------------------|----|--------------------------------|
| X | temperature (in °C) | X1 | ramp rate (in °C/min) |
| Y | derivative weight (in mg/°C) | Y2 | standard deviation of T_{ox} |

Figure B.1 — Heating rate dependence of oxidation temperature, T_{ox} , and its standard deviation σT_{ox} (inset)



Key

- | | | | |
|---|-----------------------|----|---------------------------------|
| X | ramp rate (in °C/min) | X1 | ramp rate (in °C/min) |
| Y | W_{res} (in %) | Y2 | standard deviation of W_{res} |

Figure B.2 — Heating rate dependence of the residual weight, W_{res} , and its standard deviation, σW_{res} (inset)

B.3 Sample compaction

TGA results of the “as-is” SWCNT material were compared with those of the material compacted in a standard KBr die by applying 2 t, 5 t and 10 t pressure in a hydraulic press. The values of W_{res} were essentially unaffected, while compacting at progressively higher pressure leads to a 10 °C to 20 °C decrease in the T_{ox} values. However, changes in T_{ox} do not follow a uniform trend. Compacting pressure does not affect the standard deviations of W_{res} and T_{ox} . The reason for this behaviour is not clear. It is concluded that it is better to avoid compaction, as results are difficult to predict.

B.4 Combustion

Sometimes strange and unexpected behaviour is observed in the TGA results of the SWCNT material. The weight trace suddenly goes backwards along the abscissa and then continues forward as usual. These are unambiguous signs of combustion (i.e. the sample starts rapid burning and releases a considerable amount of heat very quickly, causing a sharp increase in temperature followed by heat dissipation and a subsequent temperature drop). This behaviour is more often observed on as-produced unpurified SWCNT materials that are “fluffy” and have more metal catalyst. It is noticed that combustion decreases W_{res} and increases its standard deviation. This probably happens due to ejection of smoke particulates from the sample pan during rapid burning (i.e. there is some poorly controlled loss of mass beyond oxidation of carbon). Therefore, it is better to avoid conditions that cause combustion.

Bibliography

- [1] EBBESEN T.W., TAKADA T. Topological and SP3 defect structures in nanotubes. *Carbon*. 1995, 33, pp. 973–8
- [2] CHARLIER J.C., EBBESEN T.W., LAMBIN P. Structural and electronic properties of pentagon-heptagon pair defects in carbon nanotubes. *Phys. Rev. B*. 1996, 53, pp. 11108–13
- [3] DRESSELHAUS M.S., DRESSELHAUS G., AVOURIS P. (Eds). *Carbon Nanotubes: Synthesis, Structure, Properties and Applications*. Topics in Applied Physics. Springer-Verlag, Heidelberg, 2001
- [4] DAI H. Carbon nanotubes: opportunities and challenges. *Surface Science*. 2002, 500, pp. 218–41
- [5] ENDO M., STRANO M.S., AJAYAN P.M. Potential applications of carbon nanotubes. In: *Carbon Nanotubes: Topics in Applied Physics*. Springer-Verlag, Berlin, 2008, 111, pp. 13–61
- [6] ZHOU W., BAI X., WANG E., XIE S. Synthesis, structure, and properties of single-walled carbon nanotubes. *Advanced Materials*. 2009, 21, pp. 4568–83
- [7] ISAACS J.A., TANWANI A., HEALY M.L., DAHLBEN L.J. Economic assessment of single-walled carbon nanotube processes. *J. Nanopart. Res.* 2010, 12, pp. 551–62
- [8] MOSALA A., NASIBULIN A.G., KAUPPINEN E.I. The role of metal nanoparticles in the catalytic production of single-walled carbon nanotubes – a review. *J. Phys.: Condens. Matter*. 2003, 15, pp. S3011–35
- [9] HENNRICH F., WELLMANN R., MALIK S., LEBEDKIN S., KAPPES M.M. Reversible modification of the absorption properties of single-walled carbon nanotube thin films via nitric acid exposure. *Phys. Chem.* 2003, 5 178–83
- [10] VIGOLO B., HEROLD C., MARECHE J.F., GHANBAJA J., GULAS M., LE NORMAND F., ALMAIRAC R., ALVAREZ L., BANTIGNIES J.L. A comprehensive scenario for commonly used purification procedures of arc-discharge as-produced single-walled carbon nanotubes. *Carbon*. 2010, 48, pp. 949–63
- [11] HOU P.X., LIU C., CHENG H.M. Purification of carbon nanotubes. *Carbon*. 2008, 46, pp. 2003–25
- [12] MOON L.M., AN K.H., LEE Y.H., PARK Y.S., BAE D.J., PARK G.S. High yield purification process of singlewalled carbon nanotubes. *J. Phys. Chem. B*. 2001, 105, pp. 5677–81
- [13] MAWHINNEY D.B., NAUMENKO V., KUZNETSOVA A., YATES J.T., LIU J., SMALLEY R.E. Surface defect site density on single walled carbon nanotubes by titration. *Chemical Physics Letters*. 2001, 324, pp. 213–6
- [14] RINZLER A.G., LIU J., DAI H., NIKOLAEV P., HUFFMAN C.B., RODRIGUEZ-MACIAS E.J., BOUL P.J., LU A.H., HEYMAN D., COLBERT D.T., LEE R.S., FISCHER J.E., RAO A.M., EKLUND P.C., SMALLEY R.E. Large-scale purification of single-wall carbon nanotubes: process, product, and characterization. *Appl. Phys. A*. 1998, 67, pp. 29–37
- [15] ZHOU W., OOI Y.H., RUSSO R., PAPANEK P., LUZZI D.E., FISCHER J.E., BRONIKOWSKI M.J., WILLIS P.A., SMALLEY R.E. Structural characterization and diameter-dependent oxidative stability of single wall carbon nanotubes synthesized by the catalytic decomposition of CO. *Chem. Phys. Lett.* 2001, 350, pp. 6–14
- [16] SCHONFELDER R., RUMMELI M.H., GRUNER W., LOFFLER W., ACKER J., HOFFMANN V., GEMMING T., BUCHNER B., PICHLER T. Purification-induced sidewall functionality of magnetically pure single-walled carbon nanotubes. *Nanotechnology*. 2007, 18, pp. 375601
- [17] NIKOLAEV P., GORELIK O., ALLADA R.K., Sosa E., AREPALLI S., YOWELL L. Soft bake purification of single-walled carbon nanotubes produced by pulsed laser vaporization. *J. Phys. Chem.* 2007, 111, pp. 17678–83

- [18] MUSUMECI A.W., SILVA G.G., MARTENS W.N., WACLAWIK E.R., FROST R.L. Thermal decomposition and electron microscopy studies of single-walled carbon nanotubes. *Journal of Thermal Analysis and Calorimetry*. 2007, 88, pp. 885–91
- [19] LANDI B.J., CRESS C.D., EVANS C.M., RAFFAELLE R.R. Thermal oxidation profiling of single-walled carbon nanotubes. *Chem. Mater.* 2005, 17, pp. 6819–34
- [20] OKUBO S., SEKINE T., SUZUKI S., ACHIBA Y., TSUKAGOSHI K., AOYAGI Y., KATURA H. Purification of single-wall carbon nanotubes synthesized from alcohol by catalytic chemical vapor deposition. *Japanese Journal of Applied Physics*. 2004, 43, pp. L396–8
- [21] HOU P., LIU C., TONG Y., XU S., LIU M., CHENG H. Purification of single-walled carbon nanotubes synthesized by the hydrogen arc-discharge method. *Journal of Materials Research*. 2001, 16, pp. 2526–9
- [22] KOWALSKA E., KOWALCZYK P., RADOMSKA J., CZERWOSZ E., WRONKA H., BYSTRZEJEWSKI M. Influence of high vacuum annealing treatment on some properties of carbon nanotubes. *Journal of Thermal Analysis and Calorimetry*. 2006, 86, pp. 115–9
- [23] DERVISHI E., LI Z., WATANABE F., XU Y., SAINI V., BIRIS A.R., BIRIS A.S. Thermally controlled synthesis of single-wall carbon nanotubes with selective diameters. *Journal of Materials Chemistry*. 2009, 19, pp. 3004–12
- [24] LI H., ZHAO N., HE C., SHI C., DU X., LI J. Thermogravimetric analysis and TEM characterization of the oxidation and defect sites of carbon nanotubes synthesized by CVD of methane. *Materials Science and Engineering A*. 2008, 473, pp. 355–9
- [25] MURPHY R., COLEMAN J.N., CADEK M., MCCARTHY B., BENT M., DRURY A., BARKLIE R.C., BLAU W.J. High-yield, nondestructive purification and quantification method for multiwalled carbon nanotubes. *J. Phys. Chem. B*. 2002, 106, pp. 3087–91
- [26] BOM D., ANDREWS R., JACQUES D., ANTHONY J., CHEN B., MEIER M.S., SELEGUE J.P. Thermogravimetric analysis of the oxidation of multiwalled carbon nanotubes: evidence for the role of defect sites in carbon nanotube chemistry. *Nano Letters*. 2002, 2, pp. 615–9
- [27] MCKEE G.S.B., VECCHIO K.S. Thermogravimetric analysis of synthesis variation effects on CVD generated multiwalled carbon nanotubes. *J. Phys. Chem. B*. 2006, 110, pp. 1179–86
- [28] MCKEE G.S.B., DECK C.P., VECCHIO K.S. Dimensional control of multi-walled carbon nanotubes in floating catalyst CVD synthesis. *Carbon*. 2009, 47, pp. 2085–94
- [29] FENG Y., ZHANG H., HOU Y., MCNICHOLAS T.P., YUAN D., YANG S., DING L., FENG W., LIU J. Room temperature purification of few-walled carbon nanotubes with high yield. *ACS Nano* 2. 2008, pp. 1634–8
- [30] MANSFIELD E., KAR A., HOOKER S. Applications of TGA in quality control of SWCNTs. *Anal. Bioanal. Chem.* 2010, 396, pp. 1071–7
- [31] DECKER J.E., HIGHT WALKER A.R., BOSNICK K., CLIFFORD CA., DAI L., FAGAN J., HOOKER S., JAKUBEK Z.J., KINGSTON C., MAKAR J., MANSFIELD E., POSTEK M.T., SIMARD B., STURGEON R., WISE S., VLADAR A.E., YANG L., ZEISLER R. Sample preparation protocols for realization of reproducible characterization of single-wall carbon nanotubes. *Metrologia*. 2009, 46, pp. 682–92
- [32] MANSFIELD E., KAR A., WANG C.M., CHIARAMONTI A.N. Statistical sampling of carbon nanotube populations by thermogravimetric analysis. *Anal. Bioanal. Chem.* 2013, 405, pp. 8207–13
- [33] FREIMAN S., HOOKER S., MIGLER K., AREPALLI S. Measurement issues in single wall carbon nanotubes, NIST SP 960-19, 2008
- [34] LIMA A.M.F., MUSUMECI A.W., LIU H.W., WACLAWIK E.R., SILVA G.G. Purity evaluation and influence of carbon nanotube on carbon nanotube/graphite thermal stability. *J. Thermal. Anal. Calorim.* 2009, 97, pp. 257–63

- [35] NASA/NIST Practice Guide on Measurement Issues in Single Wall Carbon Nanotubes. Available from: <http://www.nist.gov/practiceguides>
- [36] ISO/IEC 17025, *General requirements for the competence of testing and calibration laboratories*
- [37] ISO/IEC Guide 98-3:2008, *Uncertainty of measurement — Part 3: Guide to the expression of uncertainty in measurement (GUM:1995)*

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